



Titre: Magnetless reflective gyrotropic spatial isolator metasurface
Title:

Auteurs: Guillaume Lavigne, & Christophe Caloz
Authors:

Date: 2021

Type: Article de revue / Article

Référence: Lavigne, G., & Caloz, C. (2021). Magnetless reflective gyrotropic spatial isolator metasurface. *New Journal of Physics*, 23(7), 075006 (12 pages).
Citation: <https://doi.org/10.1088/1367-2630/ac10d0>

 **Document en libre accès dans PolyPublie**
Open Access document in PolyPublie

URL de PolyPublie: <https://publications.polymtl.ca/9312/>
PolyPublie URL:

Version: Version officielle de l'éditeur / Published version
Révisé par les pairs / Refereed

Conditions d'utilisation: CC BY
Terms of Use:

 **Document publié chez l'éditeur officiel**
Document issued by the official publisher

Titre de la revue: New Journal of Physics (vol. 23, no. 7)
Journal Title:

Maison d'édition: IOP Publishing
Publisher:

URL officiel: <https://doi.org/10.1088/1367-2630/ac10d0>
Official URL:

Mention légale: Original content from this work may be used under the terms of the Creative Commons Attribution 4.0 licence. Any further distribution of this work must maintain attribution to the author(s) and the title of the work, journal citation and DOI.
Legal notice:

PAPER • OPEN ACCESS

Magnetless reflective gyrotropic spatial isolator metasurface

To cite this article: Guillaume Lavigne and Christophe Caloz 2021 *New J. Phys.* **23** 075006

View the [article online](#) for updates and enhancements.

You may also like

- [Reconfigurable chalcogenide phase change metamaterials: a material, device, and fabrication perspective](#)
Avik Mandal, Yihao Cui, Liam McRae et al.
- [Metasurfaces: a new look at Maxwell's equations and new ways to control light](#)
M A Remnev and V V Klimov
- [Resonant dielectric metasurfaces: active tuning and nonlinear effects](#)
Chengjun Zou, Jürgen Sautter, Frank Setzpfandt et al.



PAPER

Magnetless reflective gyrotropic spatial isolator metasurface

OPEN ACCESS

RECEIVED
16 April 2021REVISED
28 June 2021ACCEPTED FOR PUBLICATION
2 July 2021PUBLISHED
21 July 2021Guillaume Lavigne^{1,*}  and Christophe Caloz²¹ Electrical Engineering, Polytechnique Montréal, Montréal H3T 1J4, Canada² Faculty of Engineering Science, KU Leuven, Leuven 3000, Belgium

* Author to whom any correspondence should be addressed.

E-mail: guillaume.lavigne@polymtl.ca**Keywords:** metasurface, magnetless nonreciprocity, isolation

Original content from
this work may be used
under the terms of the
[Creative Commons
Attribution 4.0 licence](https://creativecommons.org/licenses/by/4.0/).

Any further distribution
of this work must
maintain attribution to
the author(s) and the
title of the work, journal
citation and DOI.

**Abstract**

We present the concept of a magnetless reflective gyrotropic spatial isolator (RGS) metasurface. This is a birefringent metasurface that reflects vertically polarized incident waves into a horizontally polarized waves, and absorbs horizontally polarized incident waves, hence providing isolation between the two orthogonal polarization. We first synthesize the metasurface using surface susceptibility-based generalized sheet transition conditions. We then propose a mirror-backed metaparticle implementation of this metasurface, where transistor-loaded resonators provide the desired magnetless nonreciprocal response. Finally, we demonstrate the metasurface by full-wave simulation results. The proposed RGS metasurface may be used in various electromagnetic applications, and may also serve as a step towards more sophisticated magnetless nonreciprocal metasurface systems.

1. Introduction

Nonreciprocity is a fundamental concept in science and technology [1, 2]. It allows special operations, such as isolation, circulation, nonreciprocal phase shifting and nonreciprocal gyrotropy, that are crucial in a great variety of applications. In electromagnetics, nonreciprocity is conventionally obtained through the use magnetized materials, such as ferrites [3] or terbium garnet crystals [4]. However, magnetized materials have severe drawbacks, such as incompatibility with integrated circuit technologies and bulkiness due to the required biasing magnets. Recently, the concept of magnetless nonreciprocity has arisen as a potential solution to these issues [5], with the transistor-loaded structures [6–16] and spacetime-modulated systems [17–23] being the main practical³ approaches.

Advances in magnetless nonreciprocity have recently been extended to metasurfaces, where magnetized material technologies would be inapplicable. Metasurfaces have experienced spectacular developments over the past decade [26, 27]. They have been shown to provide unprecedented control over the fundamental properties of electromagnetic waves, such as polarization, reflection, refraction, spin and orbital angular momentum. However, most of the studies on metasurfaces reported so far have focused on reciprocal structures. Introducing nonreciprocity in metasurfaces has the potential to extend conventional nonreciprocal operations such as isolation and circulation, usually applied to guided waves, to spatial wave manipulations, and to lead to novel metasurface-based wave transformations. As in other platforms, the transistor-loaded route for nonreciprocity, compared to spacetime-varying systems, has the advantage in metasurfaces to produce no spurious harmonic and intermodulation frequencies while using the simplest form of biasing, namely a simple DC battery. Transistor-loaded nonreciprocal metasurfaces have been demonstrated realizing nonreciprocal polarization rotators in reflection [9] and in transmission [10], transmissive isolation using an antenna-circuit-antenna approach [14], bianisotropic nonreciprocity [13] and meta-grating reflective circulators [16].

³ Magnetless nonreciprocity can also be obtained by nonlinearity combined by structural asymmetry [5, 24, 25]. However, the related systems are generally unpractical for engineering devices, due to major issues such as single excitation at a time, poor transmission and isolation performance, and intensity dependence.

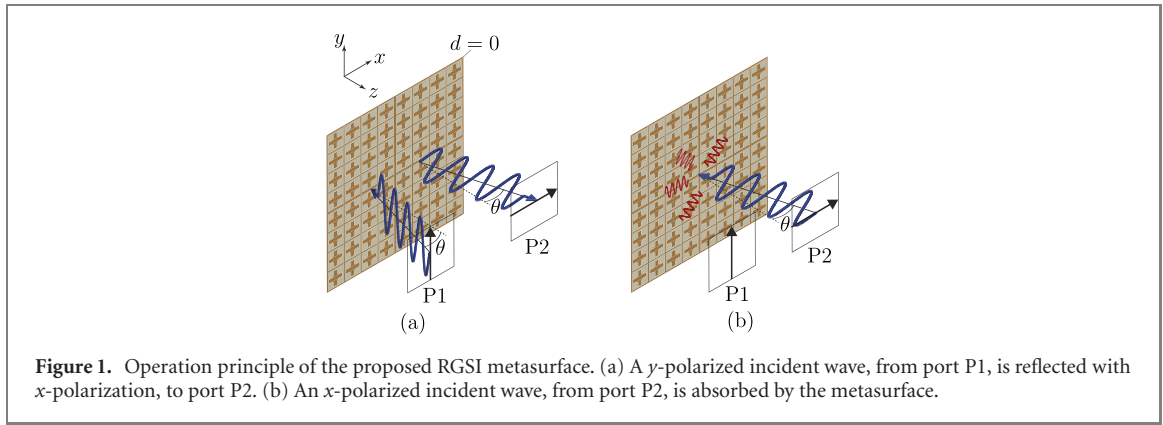


Figure 1. Operation principle of the proposed RGSI metasurface. (a) A y -polarized incident wave, from port P1, is reflected with x -polarization, to port P2. (b) An x -polarized incident wave, from port P2, is absorbed by the metasurface.

The most fundamental and primary application of nonreciprocity in metasurfaces is probably spatial isolation. Here, we introduce the concept of a reflective isolator metasurface, with a pair of orthogonally-polarized ports coupled by reflective gyrotropy, and demonstrate a corresponding magnetless reflective gyrotropic spatial isolator (RGSI).

2. Operation principle

Figure 1 depicts the operation principle of the proposed RGSI metasurface. The metasurface includes reciprocity-breaking elements, and is designed in such a manner that, using birefringence, it specularly⁴ reflects vertically-polarized incident waves into horizontally-polarized waves, as shown in figure 1(a), and absorbs horizontally-polarized incident waves, as shown in figure 1(b).

The resulting RGSI device is de facto a two-port reflective spatial isolator, with ports that we denote here P1 and P2, as indicated in the figure. Its electromagnetic response may therefore be described by the following scattering matrix:

$$\mathbf{S}_{\text{spec}}^{\text{RGSI}} = \begin{bmatrix} S_{11}^{\text{RGSI}} & S_{12}^{\text{RGSI}} \\ S_{21}^{\text{RGSI}} & S_{22}^{\text{RGSI}} \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ A e^{i\phi} & 0 \end{bmatrix}, \quad (1)$$

where A and ϕ are the amplitude and the phase, respectively, imparted by the metasurface to the rotated reflected-transmitted field. For the polarizations assumed in figure 1, the metasurface may be alternatively described by the reflection matrix

$$\mathbf{R}_{\text{spec}}^{\text{RGSI}} = \begin{bmatrix} R_{xx}^{\text{RGSI}} & R_{xy}^{\text{RGSI}} \\ R_{yx}^{\text{RGSI}} & R_{yy}^{\text{RGSI}} \end{bmatrix} = \begin{bmatrix} 0 & A e^{i\phi} \\ 0 & 0 \end{bmatrix}, \quad (2)$$

so that $\mathbf{R}_{\text{spec}}^{\text{RGSI}} = (\mathbf{S}_{\text{spec}}^{\text{RGSI}})^T$.

3. Metasurface design

3.1. GSTC equations

Metasurfaces may be modeled as zero-thickness discontinuities of space via generalized sheet transition conditions (GSTCs) and bianisotropic surface susceptibility tensors [27, 29, 30]. The GSTCs, assuming the harmonic time convention $e^{+i\omega t}$, read

$$\hat{z} \times \Delta \mathbf{H} = i\omega \mathbf{P} - \hat{z} \times \nabla M_z, \quad (3a)$$

$$\hat{z} \times \Delta \mathbf{E} = -i\omega \mathbf{M} - \frac{1}{\epsilon} \hat{z} \times \nabla P_z, \quad (3b)$$

where $\Delta \mathbf{H}$ and $\Delta \mathbf{E}$ are the differences of the magnetic or electric fields at both sides of the metasurface, and where \mathbf{P} and \mathbf{M} are the induced electric and magnetic surface polarization densities on the metasurface. The

⁴ ‘Specular’, from the Greek word ‘speculum’ that means ‘mirror’, refers to reflection that occurs under the same angle as the incidence angle, according to Snell law of reflection. We restrict here our attention to specular reflection, as implicitly assumed from the equal incidence and reflection angles (θ) in figure 1(a). However, the concept of RGSI could naturally be extended to non-specular reflection, with reflection angle differing from the incidence angle, by using metasurface gradient and bianisotropy [28].

latter may be expressed in terms of surface susceptibility tensors as

$$\mathbf{P} = \epsilon \overline{\overline{\chi}}_{ee} \mathbf{E}_{av} + k \overline{\overline{\chi}}_{em} \mathbf{H}_{av}, \quad (4a)$$

$$\mathbf{M} = k \overline{\overline{\chi}}_{me} \mathbf{E}_{av} + \mu \overline{\overline{\chi}}_{mm} \mathbf{H}_{av}, \quad (4b)$$

where \mathbf{E}_{av} and \mathbf{H}_{av} are the averages of the electric or magnetic fields at both sides of the metasurface, and $\overline{\overline{\chi}}_{ee}$, $\overline{\overline{\chi}}_{mm}$, $\overline{\overline{\chi}}_{em}$, $\overline{\overline{\chi}}_{me}$ are the 3×3 bianisotropic susceptibility tensors characterizing the metasurface. In this paper, we shall assume a purely tangential metasurface, i.e., a metasurface with $M_z = P_z = 0$, for which the bianisotropic GSTCs simplify to

$$\hat{z} \times \Delta \mathbf{H} = i\omega \epsilon \overline{\overline{\chi}}_{ee} \mathbf{E}_{av} + ik \overline{\overline{\chi}}_{em} \mathbf{H}_{av}, \quad (5a)$$

$$\Delta \mathbf{E} \times \hat{z} = ik \overline{\overline{\chi}}_{me} \mathbf{E}_{av} + i\omega \mu \overline{\overline{\chi}}_{mm} \mathbf{H}_{av}, \quad (5b)$$

where $\overline{\overline{\chi}}_{ee}$, $\overline{\overline{\chi}}_{mm}$, $\overline{\overline{\chi}}_{em}$, $\overline{\overline{\chi}}_{me}$ are now 2×2 tensors [31]. In these relations, the differences and averages of the fields are explicitly given by

$$\Delta \Phi = \Phi_t - (\Phi_i + \Phi_r), \quad (6a)$$

$$\Phi_{av} = (\Phi_t + \Phi_i + \Phi_r) / 2, \quad (6b)$$

where $\Phi = \mathbf{E}, \mathbf{H}$, where the subscript t, i and r denote the transmitted, incident and reflected fields, respectively.

3.2. Susceptibility synthesis

The metasurface can be designed using the susceptibility synthesis procedure described in [30]: (1) specify the desired field transformations, (2) compute the corresponding field differences and averages, (3) insert the expressions for these differences and averages into the susceptibility-GSTC equations, and (4) solve the resulting equations for the surface susceptibility tensors.

The GSTCs assumed here, given by (5), form a linear system of 4 scalar equations in the 16 susceptibility components containing the 4 susceptibility tensors $\overline{\overline{\chi}}_{ee}$, $\overline{\overline{\chi}}_{mm}$, $\overline{\overline{\chi}}_{em}$, and $\overline{\overline{\chi}}_{me}$ of dimensions 2×2 . The isolator operation in figure 1 involves 2 non-trivial⁵ transformations, specular gyrotropic reflection-transmission from P1 to P2, and absorption by the metasurface from P2, which implies $2 \times 4 = 8$ scalar equations in the 16 susceptibility parameters. This represents an undetermined system, requiring extra specifications for full-rank solvability. Such specifications largely depend from the specific nature of the required transformations.

The transformations in figure 1 obviously involve *gyrotropy* and *nonreciprocity*. Nonreciprocity implies $\overline{\overline{\chi}}_{ee} \neq \overline{\overline{\chi}}_{ee}^T$ or $\overline{\overline{\chi}}_{mm} \neq \overline{\overline{\chi}}_{mm}^T$ or $\overline{\overline{\chi}}_{em} \neq -\overline{\overline{\chi}}_{me}^T$ [30], where the superscript ‘T’ denotes the transpose operation, while gyrotropy implies either off-diagonal components of $\overline{\overline{\chi}}_{ee}$ and $\overline{\overline{\chi}}_{mm}$ or diagonal components of $\overline{\overline{\chi}}_{em}$ and $\overline{\overline{\chi}}_{me}$ [30]. This leaves us with several possibilities to eliminate 8 of the 16 susceptibility parameters for fully-specified resolution. We choose here, and subsequently implement, a *homoanisotropic design*, characterized by the parameters $\overline{\overline{\chi}}_{ee}$ and $\overline{\overline{\chi}}_{mm}$ with $\overline{\overline{\chi}}_{em} = \overline{\overline{\chi}}_{me} = 0$, and discuss in appendix A an alternative *bianisotropic design*⁶. We are then left with the 8 parameters, with the gyrotropy condition $\chi_{ee}^{yx}, \chi_{ee}^{xy} \neq 0$ or/and $\chi_{mm}^{yx}, \chi_{mm}^{xy} \neq 0$ and the nonreciprocal condition $\chi_{ee}^{yx} \neq \chi_{ee}^{xy}$ or/and $\chi_{mm}^{yx} \neq \chi_{mm}^{xy}$, which leads to a full-rank GSTC-susceptibility system.

Considering s-polarization (the p-polarization problem can be treated analogously) and assuming that the metasurface positioned in the plane $z = 0$, the 2 operations in figure 1 correspond to the following tangential field specifications:

$$\mathbf{E}_i = e^{-ik_0 \sin \theta x} \hat{y}, \quad \mathbf{H}_i = e^{-ik_0 \sin \theta x} \cos \theta / \eta \hat{x}, \quad (7a)$$

$$\mathbf{E}_r = A e^{-ik_0 \sin \theta x} \cos \theta e^{i\phi} \hat{x}, \quad \mathbf{H}_r = A e^{-ik_0 \sin \theta x} e^{i\phi} / \eta \hat{y}, \quad (7b)$$

$$\mathbf{E}_t = 0, \quad \mathbf{H}_t = 0, \quad (7c)$$

⁵ By ‘non-trivial’ transformations, we mean here transformations that would not be performed by the simplest metasurfaces, i.e., passive, reciprocal and nongyrotropic metasurfaces.

⁶ We follow here the convenient Greek prefix terminology used in [30], where *homo*-involves only the parameters ee and mm, *hetero*-involves only the parameters em and me, and *bi*-, introduced by Kong [32], involves both homo and hetero parameters.

where θ is the angle of incidence and reflection, for the specular gyrotropic reflection-transmission from P1 to P2, and

$$\mathbf{E}_i = \cos(-\theta)e^{-ik_0 \sin(-\theta)x}\hat{x}, \quad \mathbf{H}_i = -e^{-ik_0 \sin(-\theta)x}/\eta\hat{y}, \quad (8a)$$

$$\mathbf{E}_r = 0, \quad \mathbf{H}_r = 0, \quad (8b)$$

$$\mathbf{E}_t = 0, \quad \mathbf{H}_t = 0. \quad (8c)$$

and for the absorption by the metasurface from P2.

Substituting the field specifications (7) and (8) into (6), inserting the resulting expressions into (5), and solving for the susceptibility tensors yields the sought-after susceptibility synthesis result

$$\overline{\overline{\chi}}_{ee} = \begin{bmatrix} \chi_{ee}^{xx} & \chi_{ee}^{xy} \\ \chi_{ee}^{yx} & \chi_{ee}^{yy} \end{bmatrix} = \begin{bmatrix} \frac{-2i \sec \theta}{k} & \frac{4iA e^{i\phi}}{k} \\ 0 & \frac{-2i \cos \theta}{k} \end{bmatrix} \quad (9a)$$

$$\overline{\overline{\chi}}_{mm} = \begin{bmatrix} \chi_{mm}^{xx} & \chi_{mm}^{xy} \\ \chi_{mm}^{yx} & \chi_{mm}^{yy} \end{bmatrix} = \begin{bmatrix} \frac{-2i \sec \theta}{k} & 0 \\ \frac{4iA e^{i\phi}}{k} & \frac{-2i \cos \theta}{k} \end{bmatrix}, \quad (9b)$$

where all the components are independent from the spatial variables x and y , as might have been expected from the fact that the specified reflection is specular and hence momentum conservative.

4. Metastructure implementation

4.1. Metaparticle configuration

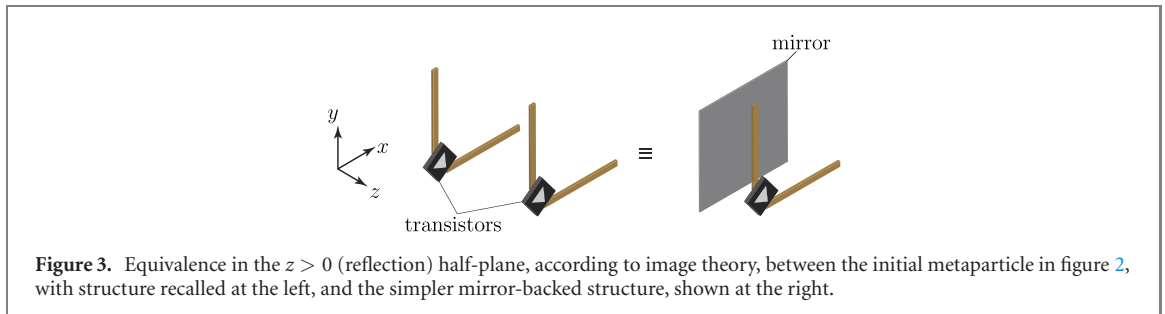
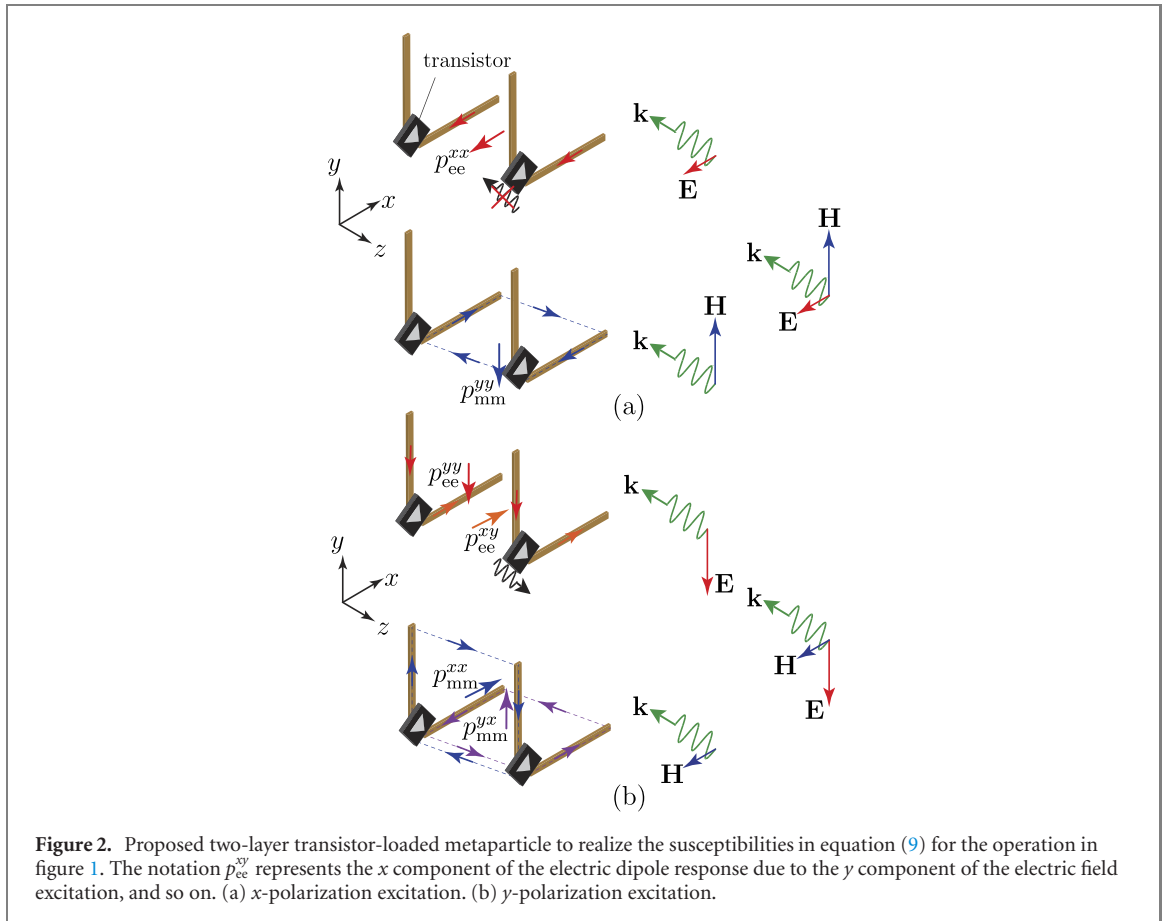
The next step of the metasurface design is naturally to implement the synthesized susceptibilities (9) in a real metasurface structure, with fully defined metaparticle material and shape, and with specific nonreciprocal elements. For the latter, we shall use here *transistors*, for their advantages of spectral purity (single-frequency operation), symmetry-breaking low-cost source (DC battery) and biasing simplicity (DC circuit). Moreover, we shall consider a normal-incidence ($\theta = 0$) design, for simplicity, but the proposed procedure and structure are easily extensible to the case of oblique incidence.

We propose the two-layer metaparticle implementation shown in figure 2 to realize the responses (9). The metaparticle structure is composed of two identical L-shaped metal resonators, each loaded by a unilateral⁷ transistor chip at the corner of the L. The transistors are biased in the non-amplifying regime where they exhibit the ideal-isolator scattering response $\mathbf{S}_{\text{tran}} = [0, 0; 1, 0]$, and they are oriented so that they pass currents flowing from the vertical section to the horizontal section and block currents flowing in the opposite direction.

Figure 2(a) depicts the response of the metaparticle to an x -polarized wave. The x -direct incident electric field induces an electric dipole moment along the x direction (χ_{ee}^{xx}), without inducing any response along the y direction due to transistor blocking ($\chi_{ee}^{yx} = 0$), while the y -directed incident magnetic field induces a magnetic dipole moment along the y direction (χ_{mm}^{yy}) without response along the x direction ($\chi_{mm}^{xx} = 0$). Figure 2(b) depicts the response of the metaparticle to a y -polarized wave. In this case, the y -directed incident electric field induces electric dipole moments along both the y and x directions (χ_{ee}^{yy} and χ_{ee}^{xy}) via the current passing across the transistor and, similarly, the x -directed incident magnetic field induces magnetic dipole moments along both the x and y directions (χ_{mm}^{xx} and χ_{mm}^{yx}). Hence, this configuration precisely provides the required non-zero and zero susceptibility components in (9).

By symmetry, the metastructure in figure 2 is in fact equivalent, on the reflection side of the metasurface, to the simpler structure where the back resonator is suppressed and replaced by a mirror placed halfway between the two initial layers, as shown in figure 3. Indeed, the latter structure, according to the image equivalence principle, exhibits the same scattering response as the former one. Given its greater simplicity, involving only one structured layer and only half the number of transistors, we shall adopt here this configuration.

⁷ In the case of a field-effect transistor, such a unilateral operation implies a common-source configuration, as typically used in RF amplifiers [33], whereas the common-gate configuration, typically used in logic electronics, is bilateral.



4.2. Metaparticle design

In the selected back-mirror metaparticle (right side in figure 3), the design task reduces to determining the layer at top of the mirror. This layer represents a metasurface per se, which is different from the overall effective metasurface that it forms with the mirror, and this layer will therefore be subsequently considered as an independent metasurface, on top of a mirror-backed substrate.

In order to account for the multiple scattering occurring between the top metasurface and the mirror, we shall use the transmission-line model [34] shown in figure 4. The metasurface and the mirror are modelled by the admittance matrices \mathbf{Y}' and \mathbf{Y}_c , respectively, and are separated by a substrate of wave impedance η_d and thickness d . The admittance matrix of the metasurface, whose parameters are to be determined, may be written as

$$\mathbf{Y}' = \begin{bmatrix} Y^{xx'} & Y^{yx'} \\ Y^{yx''} & Y^{yy''} \end{bmatrix}, \quad (10)$$

while the admittance of the mirror, which will be realized by a simple conducting copper plate, is given by

$$\mathbf{Y}_c = i\sigma\mathbf{I}, \quad (11)$$

where σ is the conductivity of the mirror, with $\sigma = 5 \times 10^7 \text{ 1}/\Omega$.

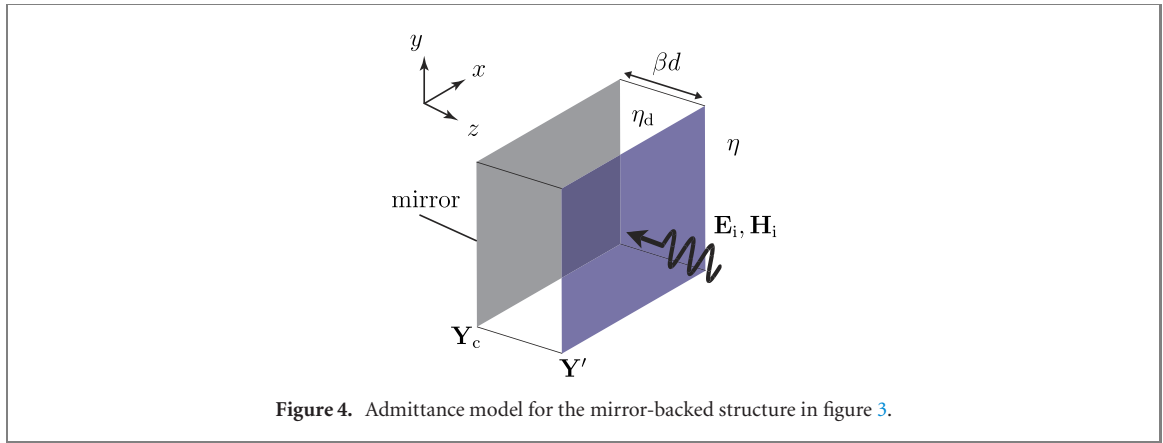


Figure 4. Admittance model for the mirror-backed structure in figure 3.

The transmission or ABCD matrix of the overall structure in figure 4 is then easily found by as

$$\begin{bmatrix} \mathbf{A} & \mathbf{B} \\ \mathbf{C} & \mathbf{D} \end{bmatrix} = \begin{bmatrix} \mathbf{I} & 0 \\ \mathbf{nY}' & \mathbf{I} \end{bmatrix} \begin{bmatrix} \mathbf{I} \cos \beta d & -\mathbf{n}i\eta_d \sin \beta d \\ \mathbf{n} \frac{i \sin \beta d}{\eta_d} & \mathbf{I} \cos \beta d \end{bmatrix} \begin{bmatrix} \mathbf{I} & 0 \\ \mathbf{nY}_c & \mathbf{I} \end{bmatrix}, \quad (12)$$

where

$$\mathbf{I} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \quad \text{and} \quad \mathbf{n} = \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} \quad (13)$$

are the identity matrix and the 90°-rotation matrix, respectively. The transmission matrix (12) can then be converted into its scattering matrix counterpart as [33]

$$\mathbf{S} = \begin{bmatrix} \mathbf{S}_{11} & \mathbf{S}_{12} \\ \mathbf{S}_{21} & \mathbf{S}_{22} \end{bmatrix} = \begin{bmatrix} -\mathbf{I} & \frac{\mathbf{Bn}}{\eta} + \mathbf{A} \\ \frac{\mathbf{n}}{\eta} & \frac{\mathbf{Dn}}{\eta} + \mathbf{C} \end{bmatrix}^{-1} \begin{bmatrix} \mathbf{I} & \frac{\mathbf{Bn}}{\eta} - \mathbf{A} \\ \frac{\mathbf{n}}{\eta} & \frac{\mathbf{Dn}}{\eta} - \mathbf{C} \end{bmatrix}, \quad (14)$$

whose \mathbf{Y}' (unknown) and other structural dependencies are naturally available from (12).

For the mirror-backed metasurface structure to realize the operation in figure 1, its reflection block, \mathbf{S}_{11} in (14), must equal the reflection matrix $\mathbf{R}_{\text{spec}}^{\text{RGSI}}$ in (2), and hence $(\mathbf{S}_{\text{spec}}^{\text{RGSI}})^T$ in (2). Enforcing this equality and solving for \mathbf{Y}' yields

$$Y^{xx'} = Y^{yy'} = \frac{\eta^2 \sin(\beta d) - \eta_d^2 \sin(\beta d) + i\eta\eta_d \cos(\beta d)}{\eta_d^2 \sigma \sin(\beta d) - \eta_d^2 \sin(\beta d) + i\eta\eta_d \cos(\beta d)}, \quad (15a)$$

$$Y^{xy'} = 2A e^{i\phi}, \quad (15b)$$

$$Y^{yx'} = 0. \quad (15c)$$

To translate this admittance matrix into metasurface susceptibilities, we write the ABCD matrix corresponding to \mathbf{Y}' as

$$\begin{bmatrix} \mathbf{A}' & \mathbf{B}' \\ \mathbf{C}' & \mathbf{D}' \end{bmatrix} = \begin{bmatrix} \mathbf{I} & 0 \\ \mathbf{nY}' & \mathbf{I} \end{bmatrix}. \quad (16)$$

convert this matrix to its scattering counterpart by reusing the formula (14), and map this matrix, which we shall call $\mathbf{S}' = [\mathbf{S}'_{11}, \mathbf{S}'_{12}; \mathbf{S}'_{21}, \mathbf{S}'_{22}]$, to the surface susceptibility matrix according to the procedure that is described in [27, 30], and that leads to the following equation:

$$\overline{\overline{\Delta}} = \overline{\overline{\chi}} \cdot \overline{\overline{A}}_v, \quad (17a)$$

where

$$\overline{\overline{\Delta}} = \begin{bmatrix} -\mathbf{m}/\eta + \mathbf{mS}'_{11}/\eta + \mathbf{mS}'_{21}/\eta & -\mathbf{m}/\eta + \mathbf{mS}'_{12}/\eta + \mathbf{mS}'_{22}/\eta \\ -\mathbf{nm} - \mathbf{nmS}'_{11} + \mathbf{nmS}'_{21} & \mathbf{nm} - \mathbf{nmS}'_{12} + \mathbf{nmS}'_{22} \end{bmatrix}, \quad (17b)$$

$$\overline{\overline{A}}_v = \frac{1}{2} \begin{bmatrix} \mathbf{I} + \mathbf{S}'_{11} + \mathbf{S}'_{21} & \mathbf{I} + \mathbf{S}'_{12} + \mathbf{S}'_{22} \\ \mathbf{n}/\eta - \mathbf{nS}'_{11}/\eta + \mathbf{nS}'_{21}/\eta & -\mathbf{n}/\eta - \mathbf{nS}'_{12}/\eta + \mathbf{nS}'_{22}/\eta \end{bmatrix} \quad (17c)$$

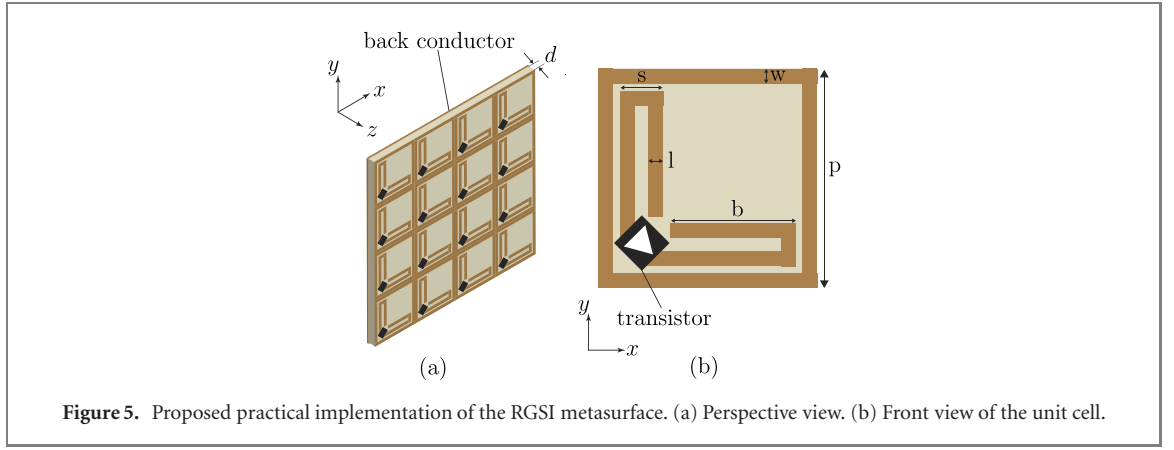


Figure 5. Proposed practical implementation of the RGSi metasurface. (a) Perspective view. (b) Front view of the unit cell.

and

$$\underline{\underline{\chi}} = \begin{bmatrix} -i\omega\epsilon\chi_{ee}^{xx'} & -i\omega\epsilon\chi_{ee}^{xy'} & -ik\chi_{em}^{xx'} & -ik\chi_{em}^{xy'} \\ i\omega\epsilon\chi_{ee}^{yx'} & i\omega\epsilon\chi_{ee}^{yy'} & ik\chi_{em}^{yx'} & ik\chi_{em}^{yy'} \\ ik\chi_{me}^{xx'} & ik\chi_{me}^{xy'} & i\omega\mu\chi_{mm}^{xx'} & i\omega\mu\chi_{mm}^{xy'} \\ -ik\chi_{me}^{yx'} & -ik\chi_{me}^{yy'} & -i\omega\mu\chi_{mm}^{yx'} & -i\omega\mu\chi_{mm}^{yy'} \end{bmatrix}, \quad (17d)$$

with

$$\mathbf{m} = \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix}. \quad (17e)$$

Substituting \mathbf{S}' into (17b) and (17c), inserting the resulting expressions into (17a), and inverting the resulting system yields the explicit susceptibility solutions, corresponding to (17d):

$$\chi_{ee}^{xx'} = \chi_{ee}^{yy'} = \frac{i}{\omega\epsilon} \frac{\eta\alpha i\zeta - \eta_d\gamma(\sigma - 1)\zeta}{\eta_d^3\gamma^2 + \eta_d^3\sigma^2\gamma^2 - 2\eta_d^3\sigma\gamma^2}, \quad (18a)$$

$$\chi_{ee}^{xy'} = \frac{i}{\omega\epsilon} 2A e^{i\phi}, \quad (18b)$$

$$\chi_{ee}^{yx'} = 0, \quad (18c)$$

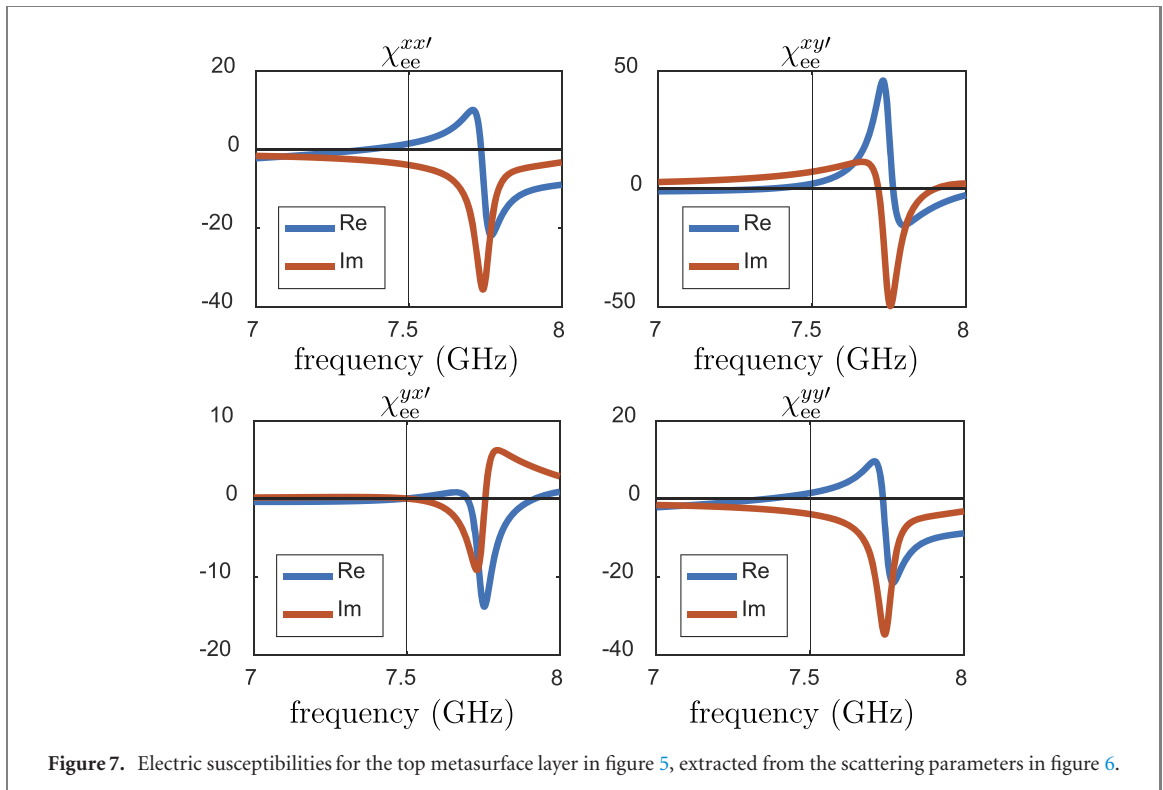
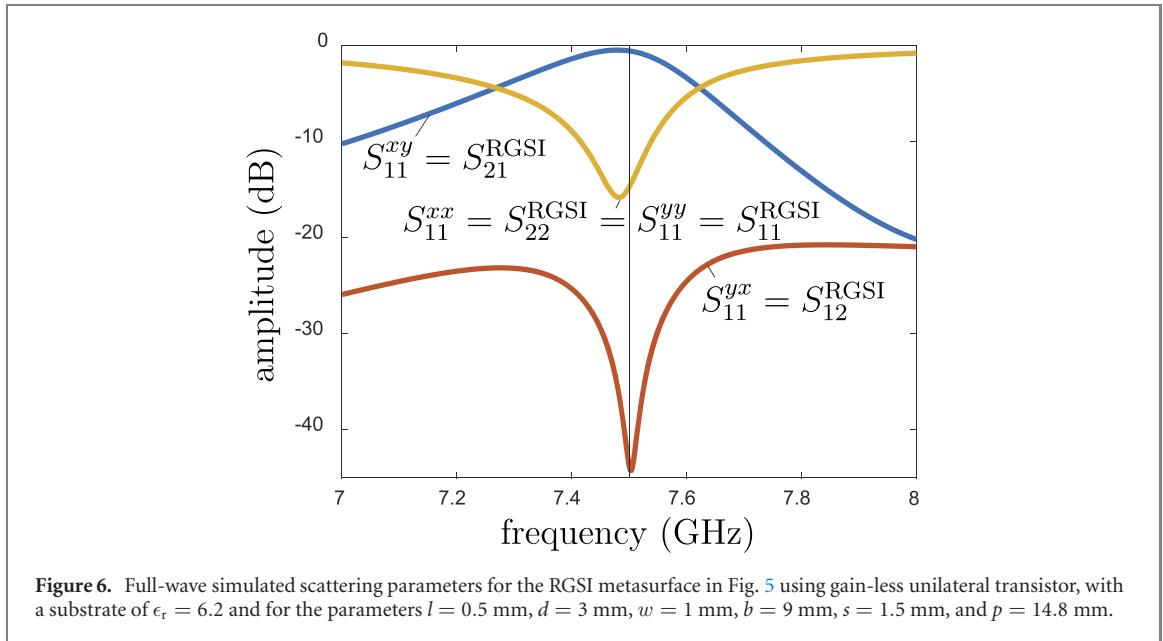
where $\alpha = \cos(\beta d)$, $\gamma = \sin(\beta d)$, $\zeta = (\eta^2\gamma - \eta_d^2\gamma + \eta_d^2\sigma\gamma + \eta\eta_d\sigma\alpha i)$ and A is the amplitude of the cross-polarized reflected wave as defined in (1). The other susceptibility tensors, $\overline{\underline{\chi}}_{mm}$, $\overline{\underline{\chi}}_{em}$ and $\overline{\underline{\chi}}_{me}$, are found to zero, which reveals that the effective tensor $\overline{\underline{\chi}}_{mm}$, required from (9b), is automatically provided by xz -loops formed between the top metasurface and the mirror, hence simplifying the former to a purely electrical homoanisotropic metasurface, characterized by the sole $\overline{\underline{\chi}}_{ee}$ susceptibility tensor.

The last step of the design is to perform geometrical-parameter full-wave simulation mapping, as described in [30]. Figure 5 shows the final metaparticle design, where we folded the strips into C-section structure for better subwavelength confinement and hence better homogenizability. Note that the currents in the parallel strips of the C-sections do not fully cancel out due to resonance non-uniformity (zero current at the edges and maximum at the center of the unfolded strip structure), which provides the same responses as those previously described despite the smaller footprint.

5. Results

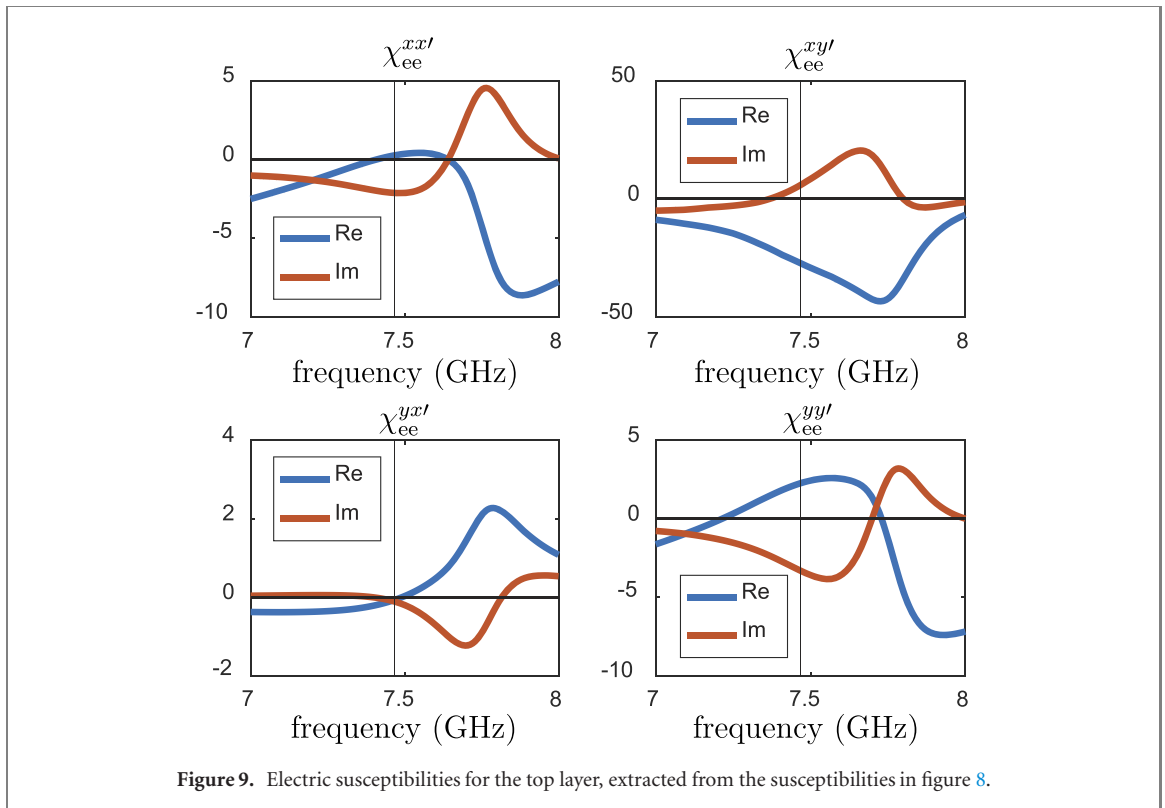
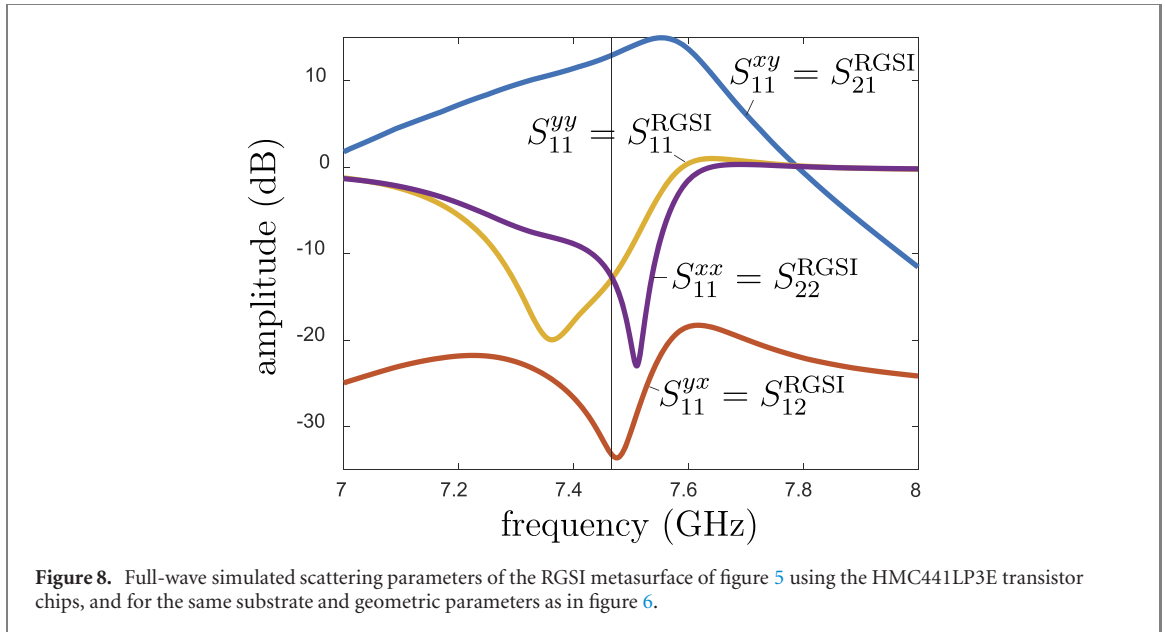
This section present full-wave simulation results, using the commercial software CST Microwave Studio, for the RGSi metasurface implementation in figure 5. We shall consider and compare two implementations: one using quasi-ideal unity-gain unilateral transistors, corresponding to a quasi-ideal isolator with scattering matrix $\mathbf{S}_{\text{trans}} = [0, I; 1, 0]$, with $I = -30$ dB, and one using the HMC441LP3E transistor chip from analog devices, with (frequency dependent) scattering parameters, including gain, given in the data sheet of the chip provided by the company. The design frequency is set to 7.5 GHz. For both implementations, we shall plot the simulated scattering parameters versus frequency, and the susceptibilities of the top layer extracted from these scattering parameters for comparison with the ideal susceptibilities given by (18)⁸.

⁸ This extraction is done, following the method described in section 4.2, as follows: (1) equating the simulated scattering matrix to the scattering matrix (14) with (12), (2) solving the resulting equations for the admittance matrix \mathbf{Y} , and (3) translating this so-obtained admittance matrix into surface susceptibilities using (16) and (17a).



Figures 6 and 7 present the results for the RGSi metasurface with the quasi-ideal unity-gain unilateral transistor. The desired RGSi operation (figure 1) is clearly observed at the design frequency (7.5 GHz) in figure 6, where the metasurface exhibits an isolation of around 40 dB between the cross-polarized ports S_{11}^{xy} and S_{11}^{yx} , and a matching of -15 dB for both co-polarized reflections. Moreover, the design results $\chi_{ee}^{xx'} = \chi_{ee}^{yy'}$ of (18a), $\chi_{ee}^{xy'} \neq 0$ of (18b) and $\chi_{ee}^{yx'} = 0$ of (18c), satisfying the nonreciprocity relation $\chi_{ee}^{yx'} \neq \chi_{ee}^{xy'}$, are verified in figure 7.

Figures 8 and 9 present the results for the RGSi metasurface with the HMC441LP3E transistor chips. The spectrum observed in figure 8 is slightly different from the design target, due to asymmetries of the chip that were not accounted for in the design; a better operation frequency here could be 7.467 GHz, which features the best trade-off between gain, isolation and matching. At this frequency, a good RGSi operation is achieved, with a gain of 13 dB (S_{11}^{xy}), an isolation of over 40 dB (with respect to S_{11}^{yx}) and equal



port matching of -12.9 dB (S_{11}^{xx} and S_{11}^{yy}). The extracted susceptibilities in figure 8, although quite different from those obtained for the uasi-ideal unilateral transistors (in figure 7), still satisfy $\chi_{ee}^{xy'} \neq 0$ of (18b) and $\chi_{ee}^{yx'} = 0$ of (18c), whereas the relation (18a) is not satisfied anymore, due the asymmetry of the transistor chip, fortunately without fatal consequence on the RGSi operation of the metasurface, as we saw in figure 8.

6. Conclusion

We have presented the concept of a magnetless RGSi metasurface. We have derived the surface susceptibility tensors required to realize this operation, and proposed a transistor-based mirror-backed implementation of a corresponding RGSi metasurface. Finally, we have demonstrated the device by full-wave simulations for both quasi-ideal unity-gain isolators and commercial transistor chips with gain. This RGSi metasurface may

be used in various electromagnetic applications and as a step towards more sophisticated magnetless nonreciprocal systems.

Data availability statement

No new data were created or analysed in this study.

Appendix A. Bianisotropic design

In section 3.2, we made the homoanisotropic choice of the 8 susceptibility components χ_{ee}^{xx} , χ_{ee}^{xy} , χ_{ee}^{yx} , χ_{ee}^{yy} , χ_{mm}^{xx} , χ_{mm}^{xy} , χ_{mm}^{yx} and χ_{mm}^{yy} to implement the proposed magnetless gyrotropic reflective spatial isolator metasurface, but we could have chosen a different set of eight susceptibility components.

Let us consider here the alternative axial bianisotropic set χ_{ee}^{xx} , χ_{ee}^{yy} , χ_{mm}^{xx} , χ_{mm}^{yy} , χ_{em}^{xx} , χ_{em}^{yy} , χ_{me}^{xx} , χ_{me}^{yy} , where the gyrotropic components are now χ_{em}^{xx} , χ_{em}^{yy} , χ_{me}^{xx} and χ_{me}^{yy} instead of χ_{ee}^{xy} , χ_{ee}^{yx} , χ_{mm}^{xy} and χ_{mm}^{yx} . Following the same procedure as in section 3.2 for this alternative set yields

$$\bar{\bar{\chi}}_{ee} = \begin{bmatrix} \chi_{ee}^{xx} & \chi_{ee}^{xy} \\ \chi_{ee}^{yx} & \chi_{ee}^{yy} \end{bmatrix} = \begin{bmatrix} \frac{-2i \sec \theta}{k} & 0 \\ 0 & \frac{-2i \cos \theta}{k} \end{bmatrix}, \quad (19a)$$

$$\bar{\bar{\chi}}_{mm} = \begin{bmatrix} \chi_{mm}^{xx} & \chi_{mm}^{xy} \\ \chi_{mm}^{yx} & \chi_{mm}^{yy} \end{bmatrix} = \begin{bmatrix} \frac{-2i \sec \theta}{k} & 0 \\ 0 & \frac{-2i \cos \theta}{k} \end{bmatrix}, \quad (19b)$$

$$\bar{\bar{\chi}}_{em} = \begin{bmatrix} \chi_{em}^{xx} & \chi_{em}^{xy} \\ \chi_{em}^{yx} & \chi_{em}^{yy} \end{bmatrix} = \begin{bmatrix} \frac{-4iA e^{i\phi} \sec \theta}{k} & 0 \\ 0 & 0 \end{bmatrix}, \quad (19c)$$

$$\bar{\bar{\chi}}_{me} = \begin{bmatrix} \chi_{me}^{xx} & \chi_{me}^{xy} \\ \chi_{me}^{yx} & \chi_{me}^{yy} \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & \frac{-4iA e^{i\phi} \cos \theta}{k} \end{bmatrix}. \quad (19d)$$

This alternative solution would naturally lead to different metaparticles than those used in the paper. Particularly, the magnetodielectric coupling terms would imply chiral, z-asymmetric metaparticles [35, 36], which could potentially be implemented by introducing transistors into chiral metaparticles similar to those in [37].

ORCID iDs

Guillaume Lavigne  <https://orcid.org/0000-0001-8235-1813>

References

- [1] Caloz C, Alù A, Tretyakov S, Sounas D, Achouri K and Deck-Léger Z-L 2018 *Phys. Rev. Appl.* **10** 047001
- [2] Asadchy V S, Mirmoosa M S, Díaz-Rubio A, Fan S and Tretyakov S A 2020 *Proc. IEEE* **108** 1684–727
- [3] Lax B and Button K J 1962 *Microwave Ferrites and Ferrimagnetics* (New York: McGraw-Hill)
- [4] Villaverde A B, Donatti D A and Bozoinis D G 1978 *J. Phys. C: Solid State Phys.* **11** L495
- [5] Caloz C and Alù A 2018 *IEEE Antennas Wirel. Propag. Lett.* **17** 1931–7
- [6] Popa B-I and Cummer S A 2007 *Microw. Opt. Technol. Lett.* **49** 2574–7
- [7] Yuan Y, Popa B-I and Cummer S A 2009 *Opt. Express* **17** 16135–43
- [8] Popa B-I and Cummer S A 2012 *Phys. Rev. B* **85** 205101
- [9] Kodera T, Sounas D L and Caloz C 2011 *Appl. Phys. Lett.* **99** 031114
- [10] Wang Z, Wang Z, Wang J, Zhang B, Huangfu J, Joannopoulos J D, Soljacic M and Ran L 2012 *Proc. Natl Acad. Sci.* **109** 13194–9
- [11] Sounas D L, Kodera T and Caloz C 2012 *IEEE Trans. Antennas Propag.* **61** 221–31
- [12] Kodera T, Sounas D L and Caloz C 2013 *IEEE Trans. Microw. Theory Tech.* **61** 1030–42
- [13] Ra'di Y and Grbic A 2016 *Phys. Rev. B* **94** 195432
- [14] Taravati S, Khan B A, Gupta S, Achouri K and Caloz C 2017 *IEEE Trans. Antennas Propag.* **65** 3589–97
- [15] Kodera T and Caloz C 2018 *IEEE Antennas Wirel. Propag. Lett.* **17** 1943–7
- [16] Ra'di Y and Alù A 2020 *Photonics* **7** 28
- [17] Hadad Y, Soric J C and Alù A 2016 *Proc. Natl Acad. Sci.* **113** 3471–5
- [18] Shi Y, Han S and Fan S 2017 *ACS Photonics* **4** 1639–45
- [19] Sounas D L, Caloz C and Alu A 2013 *Nat. Commun.* **4** 2407

- [20] Sounas D L, Estep N A, Kord A and Alù A 2018 *IEEE Antennas Wirel. Propag. Lett.* **17** 1963–7
- [21] Wang Y E 2018 *IEEE Antennas Wirel. Propag. Lett.* **17** 1973–7
- [22] Shaltout A, Kildishev A and Shalaev V 2015 *Opt. Mater. Express* **5** 2459–67
- [23] Taravati S and Eleftheriades G V 2020 *Phys. Rev. Appl.* **14** 014027
- [24] Sounas D L and Alù A 2018 *IEEE Antennas Wirel. Propag. Lett.* **17** 1958–62
- [25] Fernandes D E and Silveirinha M G 2018 *IEEE Antennas Wirel. Propag. Lett.* **17** 1953–7
- [26] Glybovski S B, Tretyakov S A, Belov P A, Kivshar Y S and Simovski C R 2016 *Phys. Rep.* **634** 1–72
- [27] Achouri K and Caloz C 2018 *Nanophotonics* **7** 1095–116
- [28] Lavigne G, Achouri K, Asadchy V S, Tretyakov S A and Caloz C 2018 *IEEE Trans. Antennas Propag.* **66** 1321–30
- [29] Achouri K, Salem M A and Caloz C 2015 *IEEE Trans. Antennas Propag.* **63** 2977–91
- [30] Achouri K and Caloz C 2020 *Electromagnetic Metasurfaces: Theory and Applications* (New York: Wiley)
- [31] Dehmollaian M, Lavigne G and Caloz C 2019 *IEEE Trans. Antennas Propag.* **67** 7396–406
- [32] Kong J A 1972 *Proc. IEEE* **60** 1036–46
- [33] Pozar D M 2011 *Microwave Engineering* 4th edn (New York: Wiley) ch 9
- [34] Pfeiffer C and Grbic A 2014 *Phys. Rev. Appl.* **2** 044011
- [35] Caloz C and Sihvola A 2020 *IEEE Antennas Propag. Mag.* **62** 58–71
- [36] Caloz C and Sihvola A 2020 *IEEE Antennas Propag. Mag.* **62** 89–98
- [37] Cheng Y, Li W and Mao X 2019 *Prog. Electromagn. Res.* **165** 35–45