

**Titre:** OpenFiberSeg : open-source segmentation of individual fibers and porosity in tomographic scans of additively manufactured short fiber reinforced composites  
**Title:**

**Auteurs:** Facundo Sosa-Rey, Yahya Abderrafai, Audrey Diouf Lewis, Daniel Therriault, Nicola Piccirelli, & Martin Lévesque  
**Authors:**

**Date:** 2022

**Type:** Article de revue / Article


**Référence:** Sosa-Rey, F., Abderrafai, Y., Diouf Lewis, A., Therriault, D., Piccirelli, N., & Lévesque, M. (2022). OpenFiberSeg : open-source segmentation of individual fibers and porosity in tomographic scans of additively manufactured short fiber reinforced composites. *Composites Science and Technology*, 226, 109497 (13 pages). <https://doi.org/10.1016/j.compscitech.2022.109497>  
**Citation:**

 **Document en libre accès dans PolyPublie**  
Open Access document in PolyPublie

**URL de PolyPublie:** <https://publications.polymtl.ca/59635/>  
**PolyPublie URL:**

**Version:** Version finale avant publication / Accepted version  
Révisé par les pairs / Refereed

**Conditions d'utilisation:** CC BY-NC-ND  
**Terms of Use:**

 **Document publié chez l'éditeur officiel**  
Document issued by the official publisher

**Titre de la revue:** Composites Science and Technology (vol. 226)  
**Journal Title:**

**Maison d'édition:** Elsevier  
**Publisher:**

**URL officiel:** <https://doi.org/10.1016/j.compscitech.2022.109497>  
**Official URL:**

**Mention légale:**  
**Legal notice:**

# OpenFiberSeg: open-source segmentation of individual fibers and porosity in tomographic scans of additively manufactured short fiber reinforced composites<sup>★</sup>

Facundo Sosa-Rey<sup>a,\*</sup>, Yahya Abderrafai<sup>a</sup>, Audrey Diouf Lewis<sup>a</sup>, Daniel Therriault<sup>a</sup>, Nicola Piccirelli<sup>b</sup> and Martin Lévesque<sup>a,\*\*</sup>

<sup>a</sup>Laboratory for Multiscale Mechanics, Polytechnique Montréal, Montreal, H3C3A7, Canada

<sup>b</sup>Safran Composites, A Technology Platform of Safran Tech, Itteville, 91760, France

## ARTICLE INFO

### Keywords:

Polymer-matrix composites (PMCs)  
Porosity/Voids  
Short-fibre composites  
X-ray computed tomography  
3-D Printing

## ABSTRACT

From a modelling standpoint, the morphology of additively manufactured (AM) high-performance short fiber reinforced polymer (SFRP) are essential to characterize, yet this task poses great challenges. The method presented extracts individual fibers from tomographic scans and produces a segmentation that is 93.1% precise on average on a per-fiber basis across a large range of fiber filling ratios (5-40 wt.%), needs minimal human input and is scalable to full-sized datasets containing  $\sim 10^5$  individual fibers. In addition, this tool allows the analysis of the correlated length and orientation distribution of fibers, and the quantification of shear-induced alignment and fiber breakage. The method is validated by successfully reproducing the segmentation of (continuous) fiber reinforced composites published in 2 separate studies and by predicting the fiber volume fraction and material density directly from the tomographic data of SFRPs. The output can serve as a basis for constituent-level mechanical modelling, and to gain insight into the relationship between processing parameters, morphology and mechanical behavior of SFRP. The full source code and imaging data are attached to this publication.

## 1. Background

Fused Filament Fabrication (FFF) is an additive manufacturing (AM) method in which parts of arbitrary geometry are built layer-by-layer. The use of materials like polyether-ether ketone (PEEK) in FFF is a very active area of research as its mechanical properties similar to human bone, its chemical and thermal resistance, biocompatibility and transparency to medical imaging methods make it a choice candidate for medical implants and prostheses [1–5]. When PEEK is used as a short fiber reinforced polymer (SFRP), the reinforcements can be oriented purposefully, enabling the engineering of parts with high weight-specific material properties [6–8]. As such, reinforced PEEK parts made by FFF are being investigated as possible replacement for heavier metallic components in the automotive and aerospace industry [5, 7–9]. However, several technical challenges complicate the printing process with this material and cause it to under-perform when compared to aircraft-grade aluminum parts [10, 11]. PEEK resin being semi-crystalline with a high melting point, significant shrinkage occurs during solidification, both of thermal origin and due to density and viscosity changes during crystallization [4, 5, 7, 8, 12]. When used in FFF, process parameters, part

<sup>★</sup> This document is the results of the research project funded by the Canadian National Science and Engineering Research Council.

\*Corresponding author

\*\*Principal corresponding author

 [facundo.sosa-rey@polymtl.ca](mailto:facundo.sosa-rey@polymtl.ca) ( Facundo Sosa-Rey); [martin.levesque@polymtl.ca](mailto:martin.levesque@polymtl.ca) ( Martin Lévesque)

ORCID(s): 0000-0003-1140-0635 ( Facundo Sosa-Rey)

38 geometry and local cooling history can interact to cause warpage of such severity as to cause print failure [8]. Adding  
39 reinforcements can reduce warpage [10] and improve mechanical properties like strength and stiffness [12], but have  
40 complex effects on crystallization [12], interlayer bonding and flow dynamics[8]. During extrusion, fibers alignment  
41 and flow characteristics are mutually dependent, and in turn affect the bonding dynamics, as fibers present at the bead  
42 surface modify diffusion conditions and surface tension [8]. Improper bonding between layers is one of the main causes  
43 why FFF parts exhibit inferior mechanical properties to molded parts, most notably across the layers [5, 12]. Porosity  
44 is another important factor, introduced both during filament production and by air trapping between passes and layers  
45 at deposition [5, 12, 13]. This reduces the effective cross-section of the parts, changes flexural properties through pore  
46 collapse, and adversely affects strength since pores act as stress concentration sites [8, 13, 14]. The inclusion of fibers  
47 has been shown to be accompanied by increased porosity [6, 9, 12, 15], measured at 20 vol.% for PEEK with 30 wt.%  
48 carbon fibers (CFs) [16]. These combined effects makes mechanical modelling of real parts a yet-unsolved challenge  
49 [8, 17–22], as all these phenomena need to be considered in concert [8]. To help address this issue, microstructural  
50 analysis methods must be developed to enable the extraction of relevant properties from imaging data, particularly at  
51 the constituent scale (single fiber and pore).

### 52 **1.1. Microstructural features**

53 In order to serve as a basis for mechanical behavior prediction, the microstructural analysis must extract the main  
54 features affecting stiffness and strength of SFRP materials (other than the inherent properties of the matrix and fibers).  
55 Those features have been identified as: the distributions of fiber lengths and orientation [23–28], the uniformity of  
56 fibers' spatial dispersion [6, 29], as well as the presence and morphology of porosity and other defects [29–32]. Unlike  
57 for the case of continuous fibers, in SFRP those properties are all affected by the processing parameters (both in  
58 injection molding or FFF) [6, 17, 25, 26, 28, 33], and are therefore crucial to understand the properties of the parts  
59 produced. For instance, shear-induced alignment of fibers and fiber breakage during the different processing steps have  
60 decisive impact on the mechanical performance of SFRP parts [6, 8].

61 Recent advances have been made on constituent-level characterization of SFRP used in FFF, for instance in basalt  
62 fiber reinforced polylactic acid (PLA) [34], and CF reinforced PEEK [16]. In both cases, proprietary software was  
63 used to perform the critical segmentation steps. Yu et al. [34] do differentiate individual fibers, but in a context of little  
64 porosity in the feedstock material (so-called inner-voids, of at most 4.2 vol.%), and moderate infill (up to 20 wt.%). As  
65 for CF reinforced PEEK, Sommacal et al. [16] centered their study on porosity distribution, and identified the volume  
66 occupied by reinforcements generally, not individual fibers.

67 In this work, we propose a method of automated constituent extraction from imaging data, called OpenFiberSeg. We  
68 draw on existing methods and techniques, complementing and adapting them to the specific case of FFF of reinforced

69 PEEK. The presence of significant porosity (~20 vol.%), low contrast in the input data and high filling ratios under  
70 consideration (up to 40 wt.%) make for a problem that is uniquely challenging. Once this problem is solved, the solution  
71 can be applied to a host of fiber reinforced materials, of equivalent or lesser degree of complexity. The intent of open  
72 distribution of both source code and imaging data guided the development of this tool, to help accelerate progress in  
73 the field.

## 74 2. Literature review

75 X-ray tomography provides volumetric renderings of the microstructure of these solids. However, since CFs  
76 and polymeric matrices have similar densities and elemental composition, the imaging data is low contrast and  
77 has considerable noise amplitude [35, 36]. As imaging apparatus are limited to a voxel size of 0.7 to 0.4  $\mu\text{m}$ , fiber  
78 identification must be performed on at best a handful of voxels, as they typically have a diameter ranging from 5 to  
79 10  $\mu\text{m}$ . Manual labelling by an expert is possible, but is a tedious, time-consuming task, and subject to inter and intra-  
80 observer variability [37]. Automatic segmentation tools are therefore required. Various groups have produced such tools  
81 for fiber-reinforced composites, the majority of which consider only two-phase materials (the phases being matrix and  
82 reinforcements) [23, 38–41]. When dealing with a third phase (the porosity), the segmentation task considered to be  
83 much harder [42, 43], especially when the grayscale values from different phases can overlap each other [43, 44] as they  
84 do in FFF reinforced PEEK. In [45], 3-phase segmentation (matrix, fibers and voids) is performed by using a stochastic  
85 optimization procedure adapted from [46, 47] to segment small regions of data, and training a neural network with the  
86 output. The authors avoid the task of manually labelling training data or the computationally prohibitive task of using  
87 the stochastic procedure on full-sized dataset. Their method performs well on real data from glass fiber reinforced  
88 polypropylene containing voids, though only visual validation is presented. Using synthetic data with no porosity, they  
89 report a per-fiber detection precision of 87.0% (651/748 fibers detected).

90 If orientation characterisation is the only concern, one traditional method is to use scanning electron microscope  
91 images of polished specimen, and determine fiber orientations based on the minor and major axes of the ellipses  
92 made by their cross-sections on the specimen surface [48]. However, this method is limited to surface level, is time-  
93 consuming, and cannot distinguish between the two orientations that produce the same elliptical cross section [36, 49].  
94 A more modern method based on 3D imaging is to compute the local orientation tensor by obtaining the local structure  
95 tensor for neighboring voxels via the Hessian matrix [24, 40, 49]. While being very general and not requiring fiber  
96 separation, this method can produce length information only for very highly resolved scans, and it is quite susceptible to  
97 noise [50] (though it can be adapted to process poorly resolved scans [39]). Furthermore, the accuracy of the orientation  
98 tensor method drops significantly if the gray intensity profile is not Gaussian inside fibers, or for high filling ratios,  
99 where fiber contact is more common [23, 24].

## 2.1. Fiber separation and tracking

To extract richer data pertaining to *individual* fibers, a necessary first step is the segmentation (labelling) of voxels belonging to fibers rather than other phases (matrix, pores, etc). Methods to perform this task include: grayscale value thresholding (Otsu's method) [38], pattern matching [51, 52], supervised machine learning (for instance K-means clustering used by Qim at DTU [53–55], or deep learning methods like those implemented in commercial software like Dragonfly™[35, 44, 50] or others. One common limitation for all these methods is that for high filling ratios, many fibers will be in close proximity, and their boundary blurred, leaving many missed detections or failing to separate distinct fibers [38, 40]. Since computer vision tools and methods are overwhelmingly aimed at 2 dimensional (2D) images, all of the cited methods are 2D-based. Many missed or false detections could be avoided by taking advantage of the 3 dimensional (3D) nature of tomographic data, but only some efforts have been made towards this goal, for instance using convolutional neural network in 3D [56, 57].

Extracting individual fibers from the voxel-wise label requires a 3D tracking procedure. A fiber tracking method proposed by Whitacre [58] (companion study of Czabaj [51]), uses template matching as the first segmentation step, then the Global Nearest Neighbor algorithm combined with the Kalman filter to estimate fiber trajectories as they are being constructed. This method also incorporates smoothing, track stitching, and a constraint by which fiber trajectories are only accepted if no volumetric overlap occurs in their paths. Whitacre reports 99.4% accuracy of track assignment, but as is pointed out, this is for a relatively small specimen (629 fibers) of *unidirectional* composite, with high scan quality. The authors recognize that for more complex, larger specimen, this method would "increase the computational cost dramatically" [51] (though mainly for the meshing and mechanical simulation than tracking *per se*). The segmentation procedure itself took 2h for 629 fibers on a desktop workstation, while 1 mm<sup>3</sup> of SFRP can contain up to  $\sim 10^5$  individual fibers [38]. Assuming linear scaling, that would translate into nearly two weeks' time.

Another tracking method applied to injected glass fiber SFRP was developed by Agyei and Sangid [38] by which the image quality of the scans are first sharpened, then voxels probably containing fibers are flagged using Otsu's method, and clustered using an iterative watershed algorithm. Ellipsoids are fitted to each cluster, and they are connected across 3D space on the basis of the proximity of their centroids. Post-processing ensures that the remaining fibers have tortuosity below a prescribed threshold. Their method successfully tracks 91 682 fibers with a processing time of 55 hrs on a desktop workstation. However, they selected injection-molded glass fiber reinforced polypropylene because of the higher contrast of glass fibers, and there is no porosity to speak of in their samples.

Partially reconstructed fibers have been stitched in different ways. Altendorf selects stitching candidates on the basis of endpoint distance, the angle between the segments, and the angle between segments and the added connecting line [59]. Creveling implement a method by which fiber tracks all considered for stitching, and the most likely candidates

131 which pass a series of checks are selected, including endpoint distance, potential interference with existing tracks, and  
132 other tests [52].

133 In FFF SFRP, the regions surrounding pores are of particular concern from a tracking standpoint. Artifacts at  
134 pore boundaries cause many missed and false detections of fibers (even for manual labelling). Hence, a heuristic that  
135 overcomes this difficulty need be more complex than those in tracking tools previously published, focused on materials  
136 with negligible porosity.

137 The ultimate objective being mechanical property inference, it is more important that the reconstructed volume be  
138 statistically equivalent to the actual solid, rather than any single fiber being found or not. As long as the proportion  
139 of phases present is correct, as well as the lengths and orientation distribution of fibers, the extracted microstructure  
140 will serve as a representative volume element [60, 61]. This guiding principle will be useful for selecting empirical  
141 parameters for aspects of our method that are probabilistic in nature, most notably the stitching partially tracked fibers.

### 142 **3. Methods**

143 In this work, contrasts in imaging data are first enhanced by histogram equalization. Then 2D-image based pre-  
144 segmentation of porosity and specimen boundary (perimeter) is performed with a combination of classical image  
145 processing (Otsu's method and Canny edge detection) and fiber regions are located with the use of a machine learning  
146 (ML) tool called InSegt [62]. From this voxel-wise labelling, a 3D-based feature extraction is performed: fiber segments  
147 are identified by locating centroids and connecting them by the K-nearest neighbor algorithm. Then, a multi-step  
148 stitching heuristic is applied to recombine these segments in a manner which can handle not only missing but also false  
149 detections. The voxel-wise labelling is then retroactively corrected to include the missing segments, and to successfully  
150 label the fiber boundaries which are a source of frequent error for ML tools. The method is shown to be effective across  
151 many material compositions (filling ratios), with close to no human input, except at the ML model training stage.

152 The material specimen under consideration here are produced by free-space extrusion (3D printing nozzle not  
153 pressed against the build plate, but extruding in air). This way, phenomena present at the meso scale (inter-bead and  
154 inter-layer voids, over- or under-extrusion) and macro scale (infill fraction, infill pattern, stacking of layers of different  
155 relative orientation, etc) [17, 18, 21, 63] are removed from consideration, allowing an analysis of the morphology at  
156 the microscale in a more pristine state.

#### 157 **3.1. Specimen preparation**

158 Pellets of PEEK 90G (Victrex™, UK) were first desiccated in a Cole-Parmer 282A Vacuum Oven (Antylia  
159 Scientific, USA) at 150°C for 5 hours. For each specimen, pellets were first introduced in a DSM Xplore Micro  
160 5 cc twin-screw microextruder (Xplore Instruments BV, Netherlands), before introduction of Panex™ 35 Type 83

161 chopped CFs (Zoltek, USA), with weight fractions from 5 to 40%, by 5% increments (pure polymer was removed  
162 from consideration as it shows no porosity and doesn't require tracking). Mixing (while extrusion is shut off) was  
163 carried out at a constant speed of 3 mm/s at 360°C. Extrusion was made at a constant speed of 3 mm/s at 390°C. Only  
164 sections of the filament with a variation of 100 microns or less as measured with a caliper were kept for extrusion in  
165 a 3D printer extruder. Printing of specimen was performed on a AON3D™ industrial 3D printer, extruding through  
166 a 0.6 mm diameter nozzle in free space (not pressing on the build plate) with a nozzle temperature of 390°C. The  
167 resulting average specimen diameter is 500  $\mu\text{m}$ .

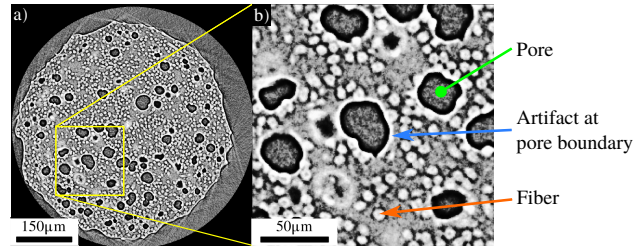
### 168 **3.2. Tomographic data acquisition**

169 Individual filaments specimens were then mounted on a pin vise and placed in a ZEISS Xradia™ 520 micro-  
170 computed tomography system. Each specimen was exposed to a source power of 80 KV, with the source at a distance  
171 of 10 mm, and the detector at 15 mm, with no filter in the beam line. 1600 projections were acquired for each specimen,  
172 for a total acquisition time of  $\sim 1.75$  hour per specimen. Volumetric reconstruction was performed with the parameters  
173 obtained automatically by the Zeiss Reconstructor™ software. The resulting voxel dimension is 0.7  $\mu\text{m}$ , and the  
174 filaments were entirely inside the scanned field of view. Figure 1a shows a sample 2D slice of the resulting tomograph,  
175 for a PEEK filament (diameter 0.6 mm) with 40 wt.% CF. In Figure 1b we can see that the pores (large dark structures)  
176 have a light region at their boundary which has the same grey intensity as the fibers (smaller white round shapes),  
177 complicating the segmentation task. These artifacts are attributed to sharp changes in refractive index in the specimen,  
178 and could be attenuated by imaging in phase-contrast mode, in which source and detector are much farther apart [64].  
179 However, this incurs much longer and therefore more expensive scans.

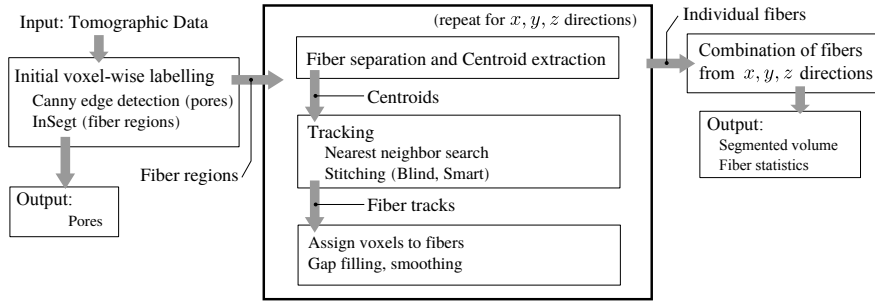
180 While OpenFiberSeg can work on larger specimen sizes (up to 1.4 mm in diameter, using 4500 projections and a  
181 total exposure time  $\sim 4$  hours), with the contrasts encountered with CF PEEK, pixel sizes  $> 1 \mu\text{m}$  lead to unsatisfactory  
182 performance of InSegt, for which the stitching procedure cannot compensate. This means highly resolved scans are  
183 required for this class of materials. Although not presently tested, glass fibers (GF) reinforcements would have a  
184 stronger imaging contrast, as they are mainly made of silicon rather than carbon atoms like polymers, have a density  
185 of 2.61  $\text{g}/\text{cm}^3$  compared to CF at 1.72  $\text{g}/\text{cm}^3$  and average diameter of 12  $\mu\text{m}$  against 7  $\mu\text{m}$  for CF [12]. In which case,  
186 larger pixel sizes (up to 2  $\mu\text{m}$ ) will probably be acceptable.

### 187 **3.3. Global processing flowchart**

188 The data processing is structured in the manner illustrated in Figure 2. Starting from the tomographic data, the  
189 phases are separated on a voxel-by-voxel basis. Then, for all three reference directions  $x$ ,  $y$  and  $z$ , individual fiber  
190 regions are separated, and centroids extracted. Tracking of fibers is performed, including stitching of partial detections.  
191 From fiber tracks, 3D representations of each fiber are constructed, with gaps identified by the stitching procedures



**Figure 1:** Sample 2D slice of tomographic scan of a PEEK 40 wt.% CF filament (after histogram equalization). a) Entire filament cross-section b) Pores and fibers are indicated by arrows, along with the artifacts in the region surrounding pores.



**Figure 2:** Schematic flowchart of the segmentation and tracking procedure. From the tomographic data, voxels containing pores and fibers are first isolated, then fibers are tracked and reconstructed from all 3 reference directions, to be combined in a single segmented microstructure.

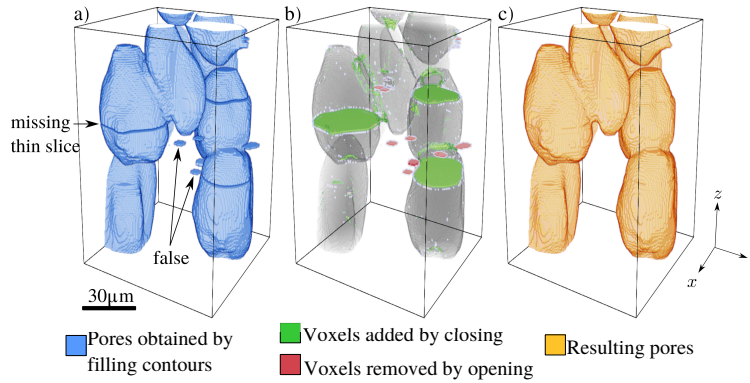
192 filled. Fibers detected from all 3 directions are then recombined to form the final segmented output. The entire procedure  
 193 requires minimal input from the user, and accomodates a variety of material types (continuous fiber composites, and  
 194 FFF SFRP of very different filling ratios, etc). The relevant parameters are scaled with respect to the voxel physical  
 195 dimension, which depend on scanning parameters.

### 196 3.4. Initial voxel-wise labelling

#### 197 3.4.1. Porosity detection

198 The first labelling steps consists in identifying which voxels contain either polymer matrix, fiber reinforcement,  
 199 porosity, or are outside the filament (the perimeter). First, the contrasts in the raw data are enhanced using histogram  
 200 equalization from the OpenCV library (`cv.equalizeHist`). Then, with the help of the Canny edge detection algorithm  
 201 (implemented in the Scikit-image library [65]), both the perimeter and the porosity can be identified on each 2D slicing  
 202 of the volume. This algorithm uses the gradient in the image and two thresholds to identify continuous contours. To  
 203 identify the perimeter, a binary mapping is first created by thresholding the image with Otsu’s method. This mapping  
 204 makes the specimen stand out from the perimeter, and the boundary is easily identified. The Canny algorithm is used  
 205 twice: on the binary mapping (to find the specimen boundary), and on the original histogram-equalized image (to  
 206 identify pore boundaries). The required parameters for the Canny algorithm depend on image characteristics. For the  
 207 datasets used in this study, the following parameters were used: `low_threshold` ranging from 60-100, `high_threshold`





**Figure 3:** Porosity labelling, typical region of data (2D slicing in  $x - y$  planes): a) as obtained by filling the closed contours of the Canny algorithm. b) Morphological closing fills in missing thin slices inside well-defined pores, opening removes false detections. c) Resulting pores.

208 of 180-200, and  $\sigma=3.0$  for the porosity detection, and  $\text{low\_threshold}=30$ ,  $\text{high\_threshold}=50$  and  $\sigma=1.0$  for  
 209 perimeter detection. See attached source code for further details. In order to fill in the closed contours in each case, the  
 210 floodfill algorithm (`cv.floodfill`) is used, which labels all the voxels reachable (not bound by a closed contour) from a  
 211 given seed point. The Canny method was favored over simpler gradient-based methods like Sobel, Roberts or Prewitt  
 212 edge detection as it more robust against noisy data [66] and it produced closed contours consistently amidst the variety  
 213 of edge characteristics encountered in the original data. As can be seen in figure 1b, pore edge sharpness can vary  
 214 significantly, making simpler methods unsuitable.

215 Figure 3a shows the result of the porosity extraction by contour filling in a typical region of data. Because the  
 216 contours are at times too attenuated in a few (typically 1-2) image slices, the volume of pores are interrupted by a few  
 217 thin missing sections. Small regions are also present, which visual inspection reveals to be false positives (the smallest  
 218 real pores are much larger than these structures which are  $<2 \mu\text{m}$  thick.)

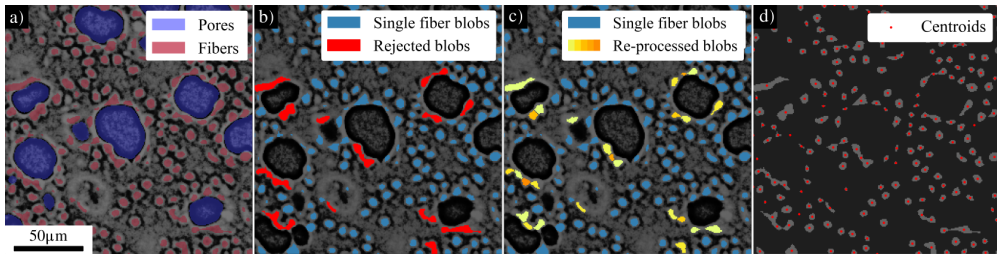
219 As shown in Figure 3b, both types of artifacts are eliminated by performing the 3D morphological operations  
 220 of **closing** (filling in missing thin slices) and **opening** (removing structures smaller than the structuring element)  
 221 as implemented in the N-dimensional image processing library `SciPy.ndimage` [67]. For both operations, spherical  
 222 structuring elements of radius 3 and 1 voxels are selected, respectively. These are large enough to handle the  
 223 encountered artifacts, and small enough to leave the general topology of pores unaffected. The resulting pores after  
 224 corrections are shown in Figure 3c. Relying on classical image processing such as this has the advantage of handling  
 225 a variety of scanning conditions and morphologies without any intervention, or occasionally requiring the adjustment  
 226 of a handful of parameters (the two Canny thresholds), rather than the re-training of neural networks encountered in  
 227 ML. We therefore elected to not investigate ML methods for this particular task.

### 3.4.2. Fiber detection and separation into convex blobs

The InSegt tool is used to find probable fiber-containing regions. In InSegt, a manual labelling of a small region of the data is used to create an image dictionary based segmentation tool using the machine-learning method called K-means clustering. A specimen image slice is then processed, yielding a probability field giving the likeliness that each voxels belongs to a fiber or not. By inspecting this probability field, the user selects a threshold above which to label pixels as fibers, and checking against the input to ensure the majority of fibers are found, with as little false positives as possible. The full volume is then processed to obtain an initial mapping of all voxels containing fibers. For specimen with low filling fraction (<15 wt.%), the fiber regions were often underestimated in size, because setting the threshold lower to capture the whole perimeter for each fiber also introduced many false detections. This minor effect was corrected with a method presented in Supplementary Materials, involving the Laplacian of the probability field.

As shown in Figure 4a, each voxel is now considered either matrix, pore, or fiber. However, the InSegt tool often labels fibers in close proximity as a single connex region, or *blob*. To identify individual fibers across the volume, it is necessary to detect the regions containing more than one fiber, and split them accordingly. First, the watershed algorithm is used to find all the connex regions (using the `cv.watershed` function, implemented in the manner detailed in [68], with distance parameter of 0.8 pixel). Then, OpenCV functions `cv.findContour` and `cv.convexityDefects` are then utilized to flag the blobs that are not convex (defined as a convexity defect size >1.2 pixels). The blobs passing or failing this convexity test are represented in Figure 4b as "single fiber" blobs and "rejected" blobs, respectively. To reprocess the "rejected" blobs, the watershed transform is used again, in a recursive manner: the distance parameter of the watershed is increased by 0.1 pixels increments for each individual blob. When the new watershed transform outputs more than one blob, the convexity test is performed on those new blobs. New blobs that are flagged as non-convex are then processed by themselves in the same manner. The resulting subdivision of each blob into the largest number of convex blobs is illustrated in Figure 4c. For these individual fiber blobs, a centroid (analogous to center of mass) is computed with the OpenCV function `cv.moments`, as shown in red in Figure 4d. Note that not all identified centroids belong to real fibers, as some will be false detections, particularly due to light-colored artifacts around pores. The shape of these artifacts is such that those centroids will most likely not form neatly defined chains of sufficient length, and they will be discarded during the tracking procedure.

The fact that detection of pores and perimeter, the splitting of blobs, the convexity tests and the extraction of centroids can be done on a slice-by-slice basis allows these step to be done in parallel, yielding a speedup factor equivalent to the number of cores available.



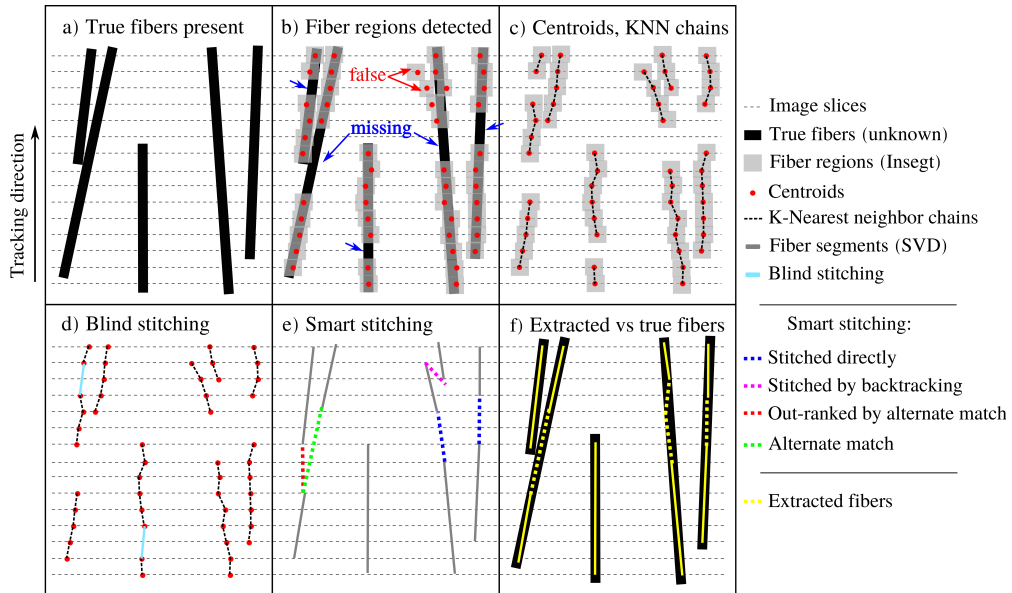
**Figure 4:** Initial labelling and centroid extraction in data from a PEEK 40 wt.% CF specimen. a) Labelling of pores by Canny edge detection and fiber blobs with InSegt. b) Fiber-containing blobs failing convexity test flagged for reprocessing. c) Output of recursive watershed transform on non-convex blobs. d) Extraction of centroids for each fiber blob.

### 3.5. Tracking

Figure 5 shows a schematic of the entire tracking procedure: image slices are imagined as 1 dimensional (1D) projections, shown as dotted lines. Fiber regions were identified (with some missing and false detections, as shown in Figure 5b, and centroids were extracted, from which complete fiber objects are sought. When tracking in the vertical direction, the fibers roughly aligned with this direction will have centroids on adjacent slices at a small distance in the transverse plane, when compared to the radius of the fibers. For each pair of adjacent slices, we want to find the pairs of centroids that are mutually closest. The K-nearest neighbor (KNN) algorithm is very efficient and highly scalable in this setting, as it can find the closest neighbor with an  $\mathcal{O}(n \log n)$  complexity. For each slice, a K-dimensional tree (KD-tree) is built (in 2D, for  $x$  and  $y$  coordinates), as implemented in SciPy. The KD-trees are then queried at the coordinates of the centroids for the following slice. We then initialize fiber objects from the continuous chains of closest centroids: centroids on the first slice which are successfully paired to those on the second form initial fiber segments (if they are within a maximum distance). From then, centroids on the following slices are either matched to an existing fiber, to which they are added, or become new fibers themselves, as depicted in Figure 5c.

#### 3.5.1. Blind stitching

Due to missing and false centroid detections, the centroid chains are often interrupted segments from a single true fiber. Using only the start- and end-points for each chain, a similar procedure is done: a 3-dimensional KDTree is constructed for the start- and end-points. Both trees are queried with the other set of points, and matching nearest neighbors are found. Three checks are made before selecting fibers for combination: these matches need be below a prescribed distance, set empirically to 2.5 fiber diameters for CF (or  $20 \mu\text{m}$ ) in the stitching direction, and 1 diameter ( $7.5 \mu\text{m}$ ) in the transverse direction, as well as to not allow backtracking: the end-point of the lowest fiber must be lower in the  $z$  direction than the start-point of the higher one. The distance criteria are taken relative to the fiber diameter, which can be measured visually if not known for a particular material. These values allows for some imprecision in the centroid position relative to the true fiber center, without allowing a match to a different fiber that is neighboring the main one. The matching pairs that meet these criteria are combined, linking the corresponding centroid chains. As



**Figure 5:** Schematic representation of fiber tracking: a) true fibers in the data (unknown). b) Detections by InSegt, with missing and false regions. c) Extracted centroids, linked in chains of nearest neighbors. d) Blind stitching: bridging small gaps of few missing centroids (light blue). e) Fiber segments that are sufficiently aligned in space are combined (blue). Segments that overlap can also be stitched, if backtracking length is below a maximum distance (shown in pink). When more than one stitching candidate is found, better alignment between longer fibers is favored (in green) over first match (in red). f) Extracted fibers overlaid on true (unknown) fibers in data.

281 we can see in Figure (5)d-e, for each centroid chain a line segment is obtained that represents its main orientation and  
 282 length, by the singular value decomposition (SVD) method (numpy.linalg.svd function).

283 The limitations of the "blind" stitching method are that if a long gap is present in the data for a particular fiber,  
 284 there isn't enough information to ascertain that the detected segments are really part of the same fiber, or if there are  
 285 two distinct fibers that are somewhat aligned. Large gaps attributable to many missing centroids are likely to occur  
 286 in two contexts: in the vicinity of pores, and when fibers that have strong inclination ( $>45^\circ$ ) relative to the main  
 287 direction, with an elongated cross-section. Both of these effects lead to interruptions in fiber tracking. With blind  
 288 stitching alone, an underestimation of long fibers would occur, and since longer fibers contribute the majority of the  
 289 mechanical load transfer, they are quite significant, especially for those at a strong inclination. To circumvent this  
 290 limitation, the following method is employed.

### 291 3.5.2. Smart stitching

292 For each fiber segment (shown in grey in Figure 5e, two six-dimensional vectors are constructed (one for each  
 293 end-point): the 3 coordinates of the point, and the 3 components of its normalized orientation vector. Then, a 6-D  
 294 KDTree is constructed for the end (topmost) points vectors, and the start (lowest) point vectors are the query points.  
 295 This way, as shown in blue in Figure 5e, we simultaneously find the pairs of objects that are closest both in terminal point

296 distance and in terms of relative angle. Here it is possible and desirable to allow the stitching of segments that exhibit  
297 backtracking: segments belonging to the same fiber overlap each other quite often, due to the presence of erroneous  
298 centroids along the path of the fiber. As shown in purple in Figure 5e, allowing the stitching of fiber segments that  
299 overlap up to a maximum prescribed distance can be done reliably by assuring that both the relative angle and the  
300 start-to-end transverse distance (in the plane normal to the main direction) are sufficiently small.

301 As shown in red in Figure 5e, sometimes a match is made first which satisfies requirements in distance and relative  
302 angle, but an alternate match (in green) is also possible, perhaps further away, but with a more perfect alignment.  
303 When instances of this scenario were encountered in the real data, predominantly the offending candidate was a short  
304 segment, in the vicinity of the endpoint of the main fiber. To avoid these false matches, a ranking function was devised  
305 that favors stitches between longer segments (the orientation vector has more statistical significance for a higher  
306 centroids count) without deteriorating the relative angle by more than a prescribed value. This way, from all possible  
307 candidate matches for a particular segment, the ones between longer segments at acceptable relative inclination were  
308 prioritized.

309 By checking not only the endpoint distance but also relative angle, the distance criteria can be set larger than for  
310 the "blind" stitching step, without risking the stitching of non-related fiber segments. Once all segments to be stitched  
311 have been identified, two additional checks are made: in the gap between the endpoints that would be connected by the  
312 stitching, new centroids are interpolated at each of the z coordinates corresponding to an image slice. Above a certain  
313 distance, to avoid connecting fibers which truly aren't related, a majority of those new centroids must be in a region  
314 which was labelled as "fiber" by the InSegt tool (rather than "pore"). Secondly, none of the new centroids can be at  
315 a distance of less than one fiber diameter from an existing fiber, as they would otherwise physically overlap with the  
316 existing fiber. If both tests are passed, stitching is allowed and the interpolated centroids are inserted in the gap between  
317 segments. Once all the stitching steps are complete, we update the fiber line segments to account for the presence of  
318 partial segments and interpolated centroids.

319 The fiber objects that have a length below a prescribed minimum are marked as "rejected". Many false positives  
320 occur at very short fiber lengths, when a few non-related centroids are connected, but do not represent a real fiber in the  
321 data. A length of 1 fiber diameter is chosen as the minimum permissible length, and fibers shorter than that are marked  
322 as "rejected". Since the mechanical behavior will be determined mainly by longer fibers, missing a few real fibers at  
323 such short length is considered acceptable, so long as the fiber filling fraction remains close to the known value for the  
324 material in question. Fibers with strong inclination ( $> 55^\circ$  from tracking direction) are also rejected, as they will be  
325 more accurately tracked along the direction with which they are most aligned with. (A vector  $[1, 1, 1]^T$  forms an angle  
326 of  $54.7^\circ$  with any of the reference axes, so a larger angle indicates better alignment with another axis). By performing

327 the entire centroid detection and tracking procedure from the 3 reference directions ( $x, y, z$ ), all possible inclinations  
328 are thus captured.

### 329 **3.6. Assigning voxels to fibers**

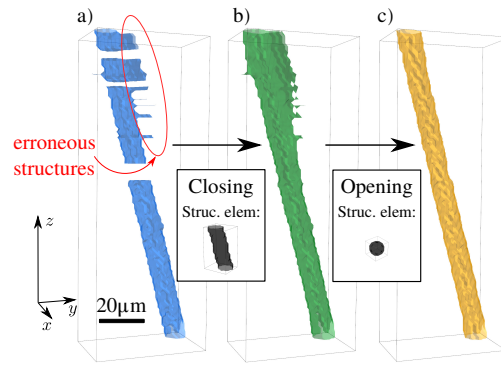
330 To reconstruct the fiber bodies from the identified centroid chains, we link voxels in the initial labelling to each  
331 of them. For the majority of voxels in the watershed output, assigning a fiber ID number is immediate, as the tracked  
332 centroid was obtained from these voxels. However, in the gaps between stitched fiber segments, the centroids created  
333 by interpolation are not related to any existing voxels. For those cases, the first step is to check whether the interpolated  
334 centroids are squarely inside a closed contour that is not already matched to another fiber, in which case all those voxels  
335 are assigned to its fiber. If more than one centroid (either interpolated or present in the initial extraction) are present  
336 in the same closed contour, the watershed transform is used to assign the voxels to the closest centroid, assuring the  
337 subdivided voxel groups all lie in a single connex region. Remains the case where interpolated centroids lie in regions  
338 where no voxels are labelled as fiber. To create this labelling, the following method is used.

### 339 **3.7. Volumetric post-processing: gap filling and artifact removal**

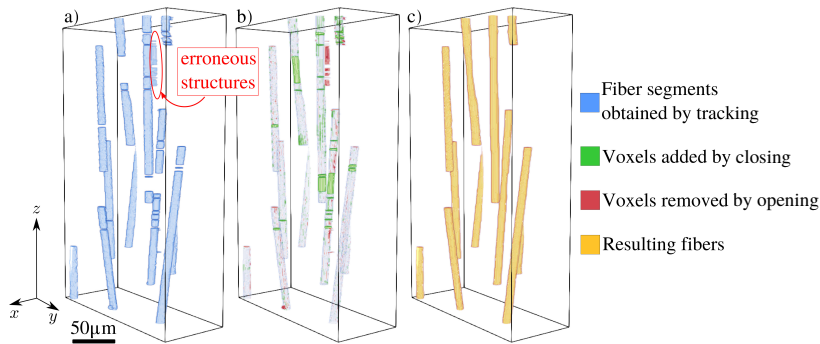
340 As shown in Figure 6a, for each fiber identified in tracking, a sub-volume is created which is only large enough to  
341 contain the voxels belonging to that fiber. A tube-like structuring element is created by stacking 2D circles (of the same  
342 diameter as a fiber) at the same angle and direction as this fiber's orientation vector, for a total height of a few voxels  
343 longer than the largest gap created by stitching (or a default value for unstitched fibers). The morphological operation of  
344 closing (`scipy.ndimage.binary_closing` function) is applied using this structuring element. As shown in Figure 6b, this  
345 has two effects: it smooths the surface of the fiber, and it fills gaps in a manner that is inferred from existing geometry,  
346 rather than prescribed. This is preferable because some fibers have an oblong rather than a circular shape, which this  
347 method preserves. Also, strongly inclined fibers will have elongated cross-sections. The morphological operation of  
348 opening (`scipy.ndimage.binary_opening`) is used afterwards with a ball structuring element, with a diameter slightly  
349 under a fiber diameter. The effect of this is to remove the regions that are erroneously labelled as belonging to this  
350 fiber: just for like pores, these false detections will be thin, and are readily removed by opening. In Figure 6c, we see  
351 the topmost regions of the fiber after removal of such an erroneous shape (i.e., an artifact).

352 Making this operation on a subset of the entire volume is memory-efficient, and can be done in parallel. A last check  
353 is made when projecting it back into the large volume: newly identified voxels should not spill into regions already  
354 identified as another fiber, or a pore.

355 In Figure 7, we can see the effect of the morphological operations on several fibers at once, in a small region of  
356 interest. In Figure 7a) are presented the fibers as obtained by tracking and assignment of voxels. We can see interruptions  
357 of different sizes, as well as the same erroneous structures previously seen. In Figure 7b the effect of closing and



**Figure 6:** Example of post-processing on a single fiber object made up of 4 stitched segments, leaving three gaps (tracking performed along  $z$ ). a) Fiber from previously labelled voxels, including erroneous structures. b) Output of morphological closing with inclined rod structuring element: gaps are filled, but erroneous regions are expanded. c) Output of morphological opening with ball structuring element: smoothing, removal of erroneous regions.



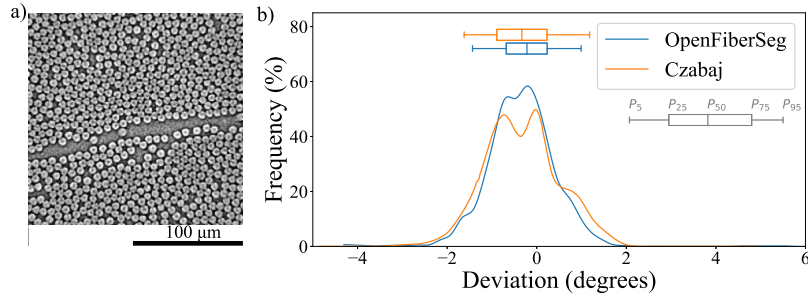
**Figure 7:** Post-processing applied to a larger region showing several distinct fiber objects. a) Fiber segments as obtained by assigning voxels to the tracking output, with several gaps. b) Morphological closing adds missing segments where interpolation has occurred, and opening removes a few erroneous structures. c) Resulting volume of fibers.

358 opening are highlighted: closing fills in the gaps between interpolated segments, opening removes erroneous regions.  
 359 The resulting fibers in Figure 7c are a much more reliable representation of those present in the data.

### 360 **3.8. Combining fibers from all reference directions ( $x, y, z$ )**

361 As strongly inclined fibers are more easily detected by slicing in the transverse plane ( $x$  and  $y$  directions), the entire  
 362 segmentation procedure explained above is repeated twice more. Using the labelling obtained in the direction of main  
 363 alignment ( $z$ ), all voxels where fibers were successfully identified (and not rejected for being too short or too steep)  
 364 are first removed from the pre-segmentation volume (subtracted from the InSegt output). This way, only new fibers  
 365 can be found.

366 After the entire procedure is performed for both  $x$  and  $y$  directions, the fibers found need to be projected onto  
 367 the original frame orientation. The most problematic cases are long fibers which are inclined by close to  $45^\circ$  to more  
 368 than one of the reference directions. This results in partial capture of segments from potentially all three reference  
 369 frames, which for the  $x$  and  $y$  directions can potentially interfere with each other. Two more steps are taken to correct



**Figure 8:** Extraction performed on original micro-CT scan of unidirectional graphite/epoxy composite. a) Sample data slice, reproduced with authorization [51]. b) Probability density function of fiber deviation from main direction, as reported by original authors, and as measured with OpenFiberSeg. The box and whisker plots for each peak represent the 5<sup>th</sup>, 25<sup>th</sup>, 50<sup>th</sup>, 75<sup>th</sup> and 95<sup>th</sup> percentiles for both segmentation methods, which are all within 0.5°, indicating good agreement between the methods.

370 these problems. First, colliding voxels are identified and if their corresponding fiber objects are sufficiently aligned,  
 371 the objects are combined into a single fiber. Then the smart stitching method is called on all the fibers from all the  
 372 permutations, with the provision that only fibers from two different permutations are eligible to be stitched together.  
 373 This allows the reconstruction of fiber whose segments were obtained from more than one reference direction. Finally,  
 374 the volumetric post-processing method is applied again on the fibers that have been combined or stitched in this last  
 375 step, yielding the final segmentation of fibers present in the data.

## 376 4. Validation

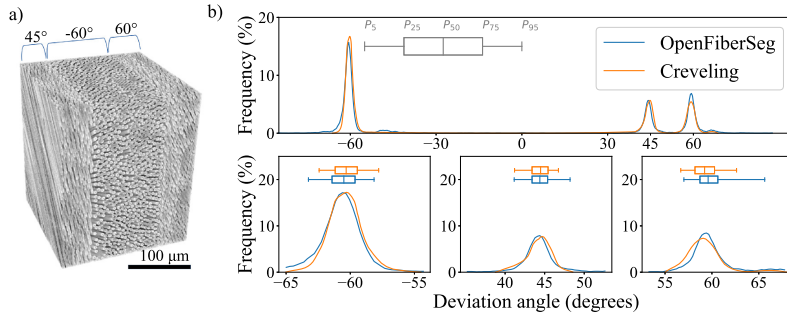
377 The segmentation procedure was performed on 2 distinct datasets, whose analysis were previously published by  
 378 Czabaj [51, 58] and Creveling [52], and kindly made available to us. By performing the segmentation on the same  
 379 input data, we can compare our tracking results to theirs, and verify the degree of accuracy of OpenFiberSeg for the  
 380 type of materials on which these scans were performed. The code from these two projects not being public, only the  
 381 results in the original publications can be discussed.

### 382 4.1. Data from Czabaj et al, 2014

383 This dataset is obtained from a specimen of AS4/35016 graphite/epoxy unidirectional composite, formed into a  
 384 thin "matchstick" specimen. The resulting tomograph is presented in Figure 8a. The authors of this work used template  
 385 matching and a sophisticated method involving the Kalman filter and track stitching to track fibers across the volume,  
 386 and preventing fiber inter-penetration [51, 58].

387 As can be seen in Figure 8b, the shape of the histograms of angles measured with our tool vs that in [51] are quite  
 388 close, especially when considering the position of the 5<sup>th</sup>, 25<sup>th</sup>, 50<sup>th</sup>, 75<sup>th</sup> and 95<sup>th</sup> percentiles, which are all within  
 389 less than 0.5° between our results and theirs. While the height of the central peak is 9% higher for our method when  
 390 compared to theirs, several reasons can account for this. When obtaining fiber centroids at each slice, we compute





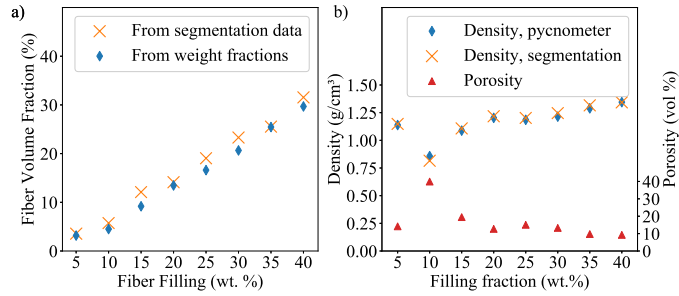
**Figure 9:** Extraction performed on micro-CT scan of carbon/epoxy laminate. a) rendering of original data, showing the main angles of the three layers, relative to the vertical direction [52]. Reproduced with authorization. b) Probability density function of fiber deviation from main direction, as reported in [52], and as measured with OpenFiberSeg. The bottom portion shows zoom around the three main peaks, with generally good agreement between the output of the two methods. The box and whisker plots for each peak represent the 5<sup>th</sup>, 25<sup>th</sup>, 50<sup>th</sup>, 75<sup>th</sup> and 95<sup>th</sup> percentiles for both segmentation methods, when grouping the data around the three main peaks.

391 the moments of the fiber blobs, whereas their methods finds the best match for a pre-defined circular template: some  
 392 variability in centroid positions is likely to occur between the two methods. Secondly, when attempting to reproduce  
 393 their results, we needed to truncate the dataset as they did, leaving 508 out of 629 fibers, without knowing the exact  
 394 coordinates. Also, while all fibers presented are found automatically in OpenFiberSeg, in the original paper manual  
 395 segmentation of 4 missed fibers, and removal of 3 false one was done. They report a processing time of 2 hours on a  
 396 CPU capable of 4 simultaneous threads. Our method also executes in 2 hours when using 4 threads.

#### 397 4.2. Data from Creveling et al. 2019

398 This data was obtained on a IM7/8552 carbon/epoxy laminate, from which a 1 mm<sup>3</sup> specimen was extracted. A  
 399 high-resolution micro-CT scan was performed, yielding a voxels size of 0.41 μm. As shown in Figure 9a, this specimen  
 400 has 3 plies, with fibers oriented at +45°, -60°, and +60°, as measured from the vertical direction. In the original paper,  
 401 the fibers were extracted using template matching and a more elaborate method of stitching. As can be seen in Figure  
 402 9b, there is only small deviation between the outputs of our method and theirs, especially when considering the position  
 403 of the percentiles for each peak. The remaining difference in peak heights can probably be explained by the different  
 404 method of obtaining centroids, i.e. template matching vs the direct calculation of center of mass of irregularly shaped  
 405 blobs, used in our method.

406 From these two analyses, we can assert that OpenFiberSeg of segmentation yields very similar results to state-of-the  
 407 art tools, at least when it comes to the tracking of fibers in bi-phasic, continuous fiber reinforced polymers. As we will  
 408 now show, OpenFiberSeg can handle a much larger number of fibers, with more randomness in orientation (hence  
 409 more contact between fibers) and to produce accurate results from partial detections, amidst porosity.



**Figure 10:** Experimental validation: a) Comparison of fiber volume fraction obtained directly from the segmentation output, vs. calculated from the known densities of matrix and reinforcement materials, as a function of fiber filling fraction. The difference between the two is at most 4% (meaning if one method gives 10%, the other can give at most 14%). b) Comparison of specimen density, as calculated from the segmentation output and the density measured directly with the help of a gas pycnometer. Very high agreement (mean error  $<2\%$ ) between the two indicates the proportions of matrix, fiber and porosity as predicted by the segmentation are a reliable indicator of the proportions in the real material.

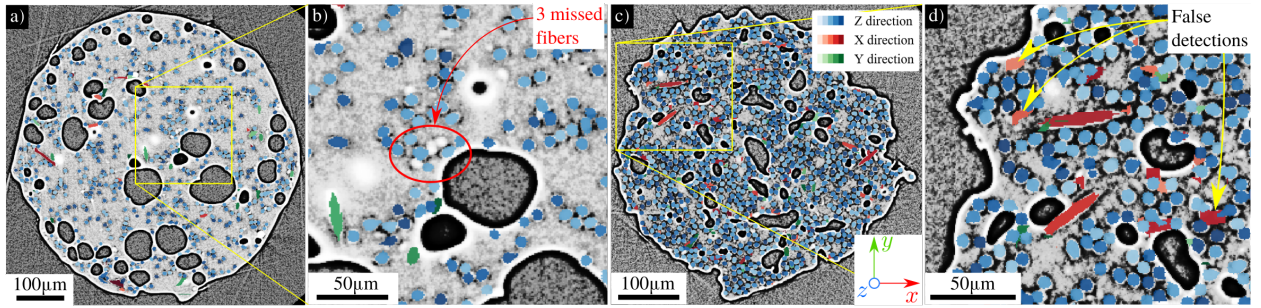
## 410 5. Results

### 411 5.1. Predicting fiber volume fraction and material density

412 For SFRP with several tens of thousands of individual fibers, getting a clear appreciation of the quality of the  
 413 segmentation is not straightforward. One way is using the segmentation data to predict properties such as the specimen  
 414 density or the fiber volume fraction  $c_f^v$  and compare them to values measured experimentally. The  $c_f^v$  is obtained directly  
 415 from segmentation data, and can be calculated experimentally from the knowledge of the mass fractions used at the  
 416 specimen preparation step, fiber and matrix density (from supplier data), and the pore volume fraction  $c_p^v$  measured  
 417 by OpenFiberSeg. To independently validate that the segmentation tool produces the correct assessment of porosity,  
 418 the total density of each SFRP specimen is calculated, and compared to the measured experimental value of density.  
 419 Detailed calculations are presented in Supplementary Materials.

420 As shown in Figure 10a, there is generally good agreements between fiber volume fractions as predicted from  
 421 the segmentation output and those obtained by the mass fractions. The results from the segmentation output are  
 422 overestimated by at most 4% for some filling fractions. This variation can be explained considering how different  
 423 are the morphologies from low to high filling fractions (with porosity ranging from 10% to 40%), and the fact that no  
 424 tweaking of parameters is done to process them.

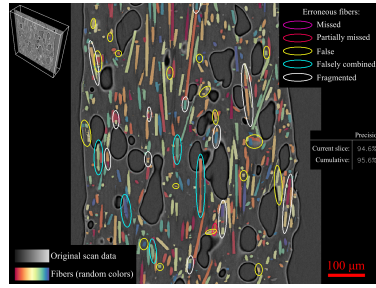
425 As shown in Figure 10b, the two methods of determining density are in high agreement (mean error of  $<2\%$ ), which  
 426 would only happen if all the volume fractions were correctly estimated, particularly  $c_p^v$ , which has a larger effect on  
 427 density, as pores occupy space but contribute no mass. Any remaining deviation between the two density measurements  
 428 can be explained by sampling error: the tomographs encompass a volume of  $1 \text{ mm}^3$ , while the specimen used for the  
 429 pycnometer measurement is  $\sim 200\times$  larger. The scanned region might possibly have a local phase distributions slightly  
 430 different from the average. The much higher porosity (39%) of the 10 wt.% CF specimen explains the large departure



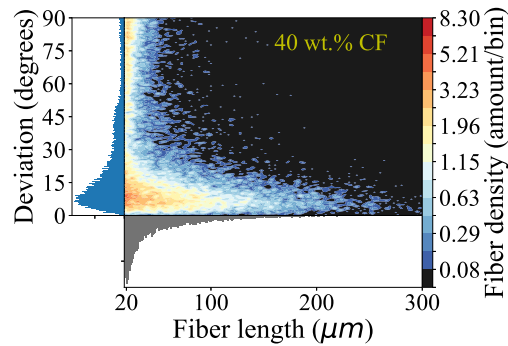
**Figure 11:** Output of segmentation for 2 material compositions: a) PEEK with 15 wt.% CF and c) with 40 wt.% CF. Different color maps are used to represent in which reference direction the fiber was detected. The majority of fibers are detected in the out-of-plane (z direction), and some in the in-plane directions x and y. In b), a closer look shows examples of missed detections, and in d), we can observe that more false detections are present in the x direction, but the strongly inclined fibers are also successfully captured.

431 of it's density from the general trend. It can also explain the largest discrepancy between both methods, at 4.9% error:  
 432 possibly some helium leaks into the unusually large pores, leading to an overestimation of density from the instrument.  
 433 Ning *et al.* also reported an uncommonly high value of porosity for 10 wt.% CF filled acrylonitrile butadiene styrene  
 434 (ABS) (9.04% whereas specimen with 0-15% filling averaged at 2%) [31].

435 It remains possible however that the volume fractions are accurate on average, but only due to the number of  
 436 missed fiber detections being cancelled by false detections. To ascertain how reliable the output at the pixel level, the  
 437 following method is used. On a slice-by-slice basis, we can superimpose the segmentation output onto the raw data.  
 438 This visualization is presented in Figure 11 for two different material composition: in a) PEEK with 15 wt.% CF and in  
 439 b) PEEK with 40 wt.% CF. A different colormap was used to show which reference direction each fiber was detected  
 440 from. For both these materials, it is clearly visible that the vast majority of fibers present are identified, with only a  
 441 few missed fibers or false detections. Also, nearly full cross-section of each fiber is captured rather than a portion of  
 442 it. And while there are more false detections in the in-plane directions (as shown in Figure 11d), the fibers with strong  
 443 inclination (near-tangent to the  $x - y$  plane) are also successfully captured. To assess the segmentation precision, a  
 444 slice-by-slice analysis is presented in Video 1 for the specimen with 25 wt.% CF. For each studied slice, we compared  
 445 the fibers detected by OpenFiberSeg against the original data, and labelled false fibers or single true fibers fragmented  
 446 into segments as false positives (FP) and missed fibers or separate true fibers combined into one as false negative  
 447 (FN). This annotation is performed at 7 separate locations (2D slices) in the data, encompassing 3945 individual fiber  
 448 detections. Precision for this specimen (defined as the voxel ratio of  $TP/(TP+FP)$ ) is computed to 95.6%, with rates of  
 449 FP of 4.4% and FN of 1.6% (average across all filling ratios: precision: 93.1%, FP: 6.9%, FN: 1.5%). The majority of FP  
 450 are in the vicinity of pores, and are for short fibers ( $<20 \mu\text{m}$ ). Overall, there is  $<1\%$  occurrence of fiber fragmentation  
 451 or false combination.



**Video 1:** Slice-by-slice analysis of segmentation accuracy: PEEK 25 wt.% CF. The porosity and perimeter detection are shown to be nearly perfect. The fiber extraction precision is measured at 95.6% for this specimen. Animated sweep of fibers colored first by length and then deviation highlight the trend by which longer fibers are better aligned and vice-versa.

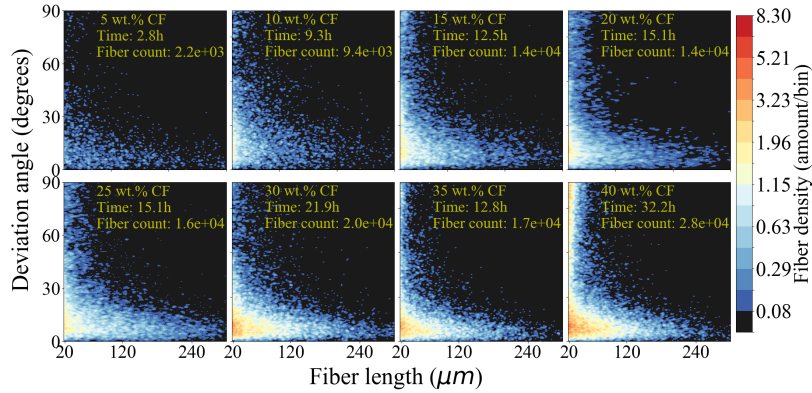


**Figure 12:** 2D histogram representation of the correlated lengths and angle of deviation from tracking direction ( $z$ ) for fibers present in a PEEK specimen with 40 wt.% CF filling ratio. Single-variable histograms are juxtaposed on the left-hand and lower side, to highlight the relationship between the counts for each variable and the correlated density values.

## 452 5.2. Discussion

453 For each material specimen, we obtain a set of individual fibers, complete with their position in space, orientation  
 454 vector and length. In order to study the correlated distribution of lengths and orientations, and to compare them across  
 455 material composition, we produce the following visualization. In Figure 12, a 2D-histogram is presented for the fibers  
 456 present in a PEEK specimen with 40 wt.% CF. The lengths and deviation angle are both discretized into 256 bins,  
 457 and the color of each pixel represents the density (amount/bin) for that combination of length and deviation angle. A  
 458 logarithmic scale is used for the colormap, so that both high and low density regions are appreciable. Single-variable  
 459 histograms for lengths and deviation angle are also shown, making explicit the relation between bin count and the pixel  
 460 color mapping. The correlated histogram allows us to assert the inverse relation between fiber length and deviation:  
 461 longer fibers tend to be better aligned, and shorter fibers can deviate more (although the bulk of the distribution is  
 462 always at  $<30^\circ$ ). The extent of shear-induced alignment during the extrusion process is thus revealed, which could not  
 463 have been inferred from the single-variable histograms alone.

464 The same visualization allows us to compare the specimen between them: in Figure 13, all 8 specimen types are  
 465 juxtaposed, in order of increasing filling ratio. Fiber counts and processing times on a workstation with an Intel™



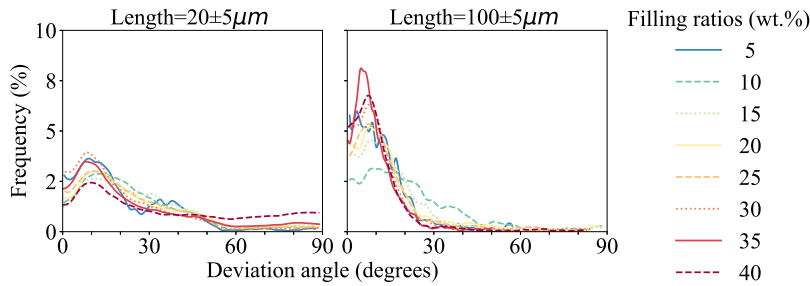
**Figure 13:** Correlated lengths and deviation histograms for PEEK SFRP with filling ratios of 5-40 wt.% CF. For all levels of filling, there exists an inverse correlation between fiber length and deviation: longer fibers will be more aligned with the extrusion direction. Processing time is given, along with fiber count for each scan.

466 i9-10940X CPU, and 64GB of RAM are presented for each dataset. Here we can see that the shear-induced alignment  
 467 is present even at low fiber concentrations. This indicates it is attributable to fibers aligning with the flow direction,  
 468 more than interactions between fibers which are less frequent at low filling fraction. Also, for higher ratios, the most  
 469 noticeable increase (regions in red) is in the  $<100 \mu\text{m}$ ,  $<30^\circ$  range, suggesting more fiber breakage at these ratios, as  
 470 the proportion of fibers  $100 \mu\text{m}$  and longer are essentially the same for 30 wt.% CF and above. The unusually large  
 471 proportion of short fibers at large deviations for the 40 wt.% CF also suggest more breakage for higher filling ratios.  
 472 Additionally, the lower fiber count at 35 wt.% compared to 30 wt.% suggests there is less fiber breakage at this filling  
 473 ratio.

474 The degree to which shear-induced alignment is more pronounced for longer fibers is illustrated in Figure 14.  
 475 Here, for each dataset, only the fibers of a certain length are selected (centered at 20 and  $100 \mu\text{m}$ ) and the histograms  
 476 of the deviation angles are compared. Clearly, the general tendency is that fibers tend to align with the flow direction  
 477 (the bulk of the distribution is always at  $>30^\circ$ ) but this phenomenon is markedly more prominent as longer fibers are  
 478 considered. One dataset (10 wt.% CF) doesn't follow this trend, which can be explained by inordinately large porosity  
 479 for this specimen, probably changing the flow characteristics. The highest peak for long ( $100 \mu\text{m}$ ) fibers being for the  
 480 35 wt.% also indicates less fiber breakage at this filling ratio.

## 481 6. Conclusion

482 In this work, we presented OpenFiberSeg, a tool for fiber tracking and segmentation of individual fibers in  
 483 tomographic scans of SFRPs. Combining elements from several techniques, we propose original improvements such as  
 484 retroactive correction of labelling based on fiber reconstruction, as well as a detailed heuristic for stitching fibers from  
 485 partially detected segments. The method is shown to be robust and satisfactorily reproduces the results of 2 independent



**Figure 14:** Histograms of deviation angles for 2 different ranges of fiber lengths, centered at 20 and 100  $\mu\text{m}$ , by specimen filling fraction. Shear-induced alignment is present for all specimen, as evidenced by the bulk of the distribution being below 30° for specimen. This effect is more pronounced for longer fibers for all filling ratios, except 10 wt.%, which can be explained by unusually high porosity.

486 studies on continuous fiber reinforced composites. When applied to FFF SFRP with non-negligible porosity, it can be  
 487 used to corroborate the experimental measurement of porosity and fiber filling fraction, and produce a detailed portrait  
 488 of the correlated fiber lengths and orientation distributions for vastly dissimilar specimen composition (5-40 wt.%  
 489 filling ratio), yielding an average segmentation precision of 93.1% on a per-voxel basis. This tool can serve as a central  
 490 characterization and diagnostic method for the development of FFF SFRP materials and processes. However, it is not  
 491 designed for fibers with significant curvature, as fibers are represented by line segments, and up to 1% of fibers can be  
 492 fragmented or combined with another with which they are well aligned and in close proximity. By divulging the source  
 493 code, this project can reduce development time for other research groups, and be applied to a variety of use cases, such  
 494 as other types of SFRP, reinforced ceramics, concrete, etc. The precise knowledge of reinforcement and pore size and  
 495 position will be invaluable for the development of models involving elasticity, viscoelasticity, fracture dynamics, and  
 496 transport phenomena.

## 497 7. Source code and data repository

498 The full source code repository along with original tomographic data used in this work are available at <https://github.com/lm2-poly/OpenFiberSeg>.  
 499

## 500 Acknowledgements

501 This research project is made possible by financial and technical support from Safran S.A. (FACMO Research  
 502 Chair), as well as financial support from the Natural Sciences and Engineering Research Council of Canada (Alexander  
 503 Graham Bell Canada Graduate Scholarship program, and the Collaborative Research and Development program, grant  
 504 no CRDPJ514761). Computational resources were made available by Calcul Québec ([www.calculquebec.ca](http://www.calculquebec.ca)) and  
 505 Compute Canada ([www.computecanada.ca](http://www.computecanada.ca)). Research data used for validating the accuracy of our method was shared  
 506 with us by Pr. Czabaj at the University of Utah.

## References

- 507
- 508 [1] R. Dua, Z. Rashad, J. Spears, G. Dunn, M. Maxwell, Applications of 3d-printed peek via fused filament fabrication: A systematic review,  
509 Polymers 13 (2021) 4046.
- 510 [2] A. Haleem, M. Javaid, Polyether ether ketone (peek) and its manufacturing of customised 3d printed dentistry parts using additive  
511 manufacturing, Clinical Epidemiology and Global Health 7 (2019) 654–660.
- 512 [3] L. Ding, W. Lu, J. Zhang, C. Yang, G. Wu, Preparation and performance evaluation of duotone 3d-printed polyetheretherketone as oral  
513 prosthetic materials: A proof-of-concept study, Polymers 13 (2021) 1949.
- 514 [4] W. Wu, P. Geng, J. Zhao, Y. Zhang, D. Rosen, H. Zhang, Manufacture and thermal deformation analysis of semicrystalline polymer polyether  
515 ether ketone by 3d printing, Materials Research Innovations 18 (2014) S5–12.
- 516 [5] P. Wang, B. Zou, H. Xiao, S. Ding, C. Huang, Effects of printing parameters of fused deposition modeling on mechanical properties, surface  
517 quality, and microstructure of peek, Journal of Materials Processing Technology 271 (2019) 62–74.
- 518 [6] H. L. Tekinalp, V. Kunc, G. M. Velez-Garcia, C. E. Duty, L. J. Love, A. K. Naskar, C. A. Blue, S. Ozcan, Highly oriented carbon fiber–polymer  
519 composites via additive manufacturing, Composites Science and Technology 105 (2014) 144–150.
- 520 [7] R. Gao, J. Xie, J. Yang, C. Zhuo, J. Fu, P. Zhao, Research on the fused deposition modeling of polyether ether ketone, Polymers 13 (2021)  
521 2344.
- 522 [8] B. Brenken, E. Barocio, A. Favaloro, V. Kunc, R. B. Pipes, Fused filament fabrication of fiber-reinforced polymers: A review, Additive  
523 Manufacturing 21 (2018) 1–16.
- 524 [9] M. Rinaldi, F. Cecchini, L. Pigliaru, T. Ghidini, F. Lumaca, F. Nanni, Additive manufacturing of polyether ether ketone (peek) for space  
525 applications: A nanosat polymeric structure, Polymers 13 (2021) 11.
- 526 [10] L. J. Love, V. Kunc, O. Rios, C. E. Duty, A. M. Elliott, B. K. Post, R. J. Smith, C. A. Blue, The importance of carbon fiber to polymer additive  
527 manufacturing, Journal of Materials Research 29 (2014) 1893–1898.
- 528 [11] M. Luo, X. Tian, J. Shang, W. Zhu, D. Li, Y. Qin, Impregnation and interlayer bonding behaviours of 3d-printed continuous carbon-fiber-  
529 reinforced poly-ether-ether-ketone composites, Composites Part A: Applied Science and Manufacturing 121 (2019) 130–138.
- 530 [12] P. Wang, B. Zou, S. Ding, C. Huang, Z. Shi, Y. Ma, P. Yao, Preparation of short cf/gf reinforced peek composite filaments and their  
531 comprehensive properties evaluation for fdm-3d printing, Composites Part B: Engineering 198 (2020) 108175.
- 532 [13] Stepashkin, D. Chukov, F. Senatov, A. Salimon, A. Korsunsky, S. Kaloshkin, 3d-printed peek-carbon fiber (cf) composites: Structure and  
533 thermal properties, Composites Science and Technology 164 (2018) 319–326.
- 534 [14] Q. Li, W. Zhao, Y. Li, W. Yang, G. Wang, Flexural properties and fracture behavior of cf/peek in orthogonal building orientation by fdm:  
535 Microstructure and mechanism, Polymers 11 (2019) 656.
- 536 [15] L. Pigliaru, M. Rinaldi, L. Ciccacci, A. Norman, T. Rohr, T. Ghidini, F. Nanni, 3d printing of high performance polymer-bonded peek-ndfeb  
537 magnetic composite materials, Functional Composite Materials 1 (2020) 1–17.
- 538 [16] S. Sommacal, A. Matschinski, K. Drechsler, P. Compston, Characterisation of void and fiber distribution in 3d printed carbon-fiber/peek using  
539 x-ray computed tomography, Composites Part A: Applied Science and Manufacturing (2021) 106487.
- 540 [17] S. Garzon-Hernandez, A. Arias, D. Garcia-Gonzalez, A continuum constitutive model for fdm 3d printed thermoplastics, Composites Part B:  
541 Engineering 201 (2020) 108373.
- 542 [18] A. Nasirov, A. Gupta, S. Hasanov, I. Fidan, Three-scale asymptotic homogenization of short fiber reinforced additively manufactured polymer  
543 composites, Composites Part B: Engineering 202 (2020) 108269.

- 544 [19] M. Somireddy, A. Czekanski, Computational modeling of constitutive behaviour of 3d printed composite structures, *Journal of Materials*  
545 *Research and Technology* 11 (2021) 1710–1718.
- 546 [20] W. Gao, Y. Zhang, D. Ramanujan, K. Ramani, Y. Chen, C. B. Williams, C. C. Wang, Y. C. Shin, S. Zhang, P. D. Zavattieri, The status,  
547 challenges, and future of additive manufacturing in engineering, *Computer-Aided Design* 69 (2015) 65–89.
- 548 [21] M. Domingo-Espin, J. M. Puigoriol-Forcada, A.-A. Garcia-Granada, J. Llumà, S. Borros, G. Reyes, Mechanical property characterization and  
549 simulation of fused deposition modeling polycarbonate parts, *Materials & Design* 83 (2015) 670–677.
- 550 [22] M. Talagani, S. DorMohammadi, R. Dutton, C. Godines, H. Baid, F. Abdi, V. Kunc, B. Compton, S. Simunovic, C. Duty, et al., Numerical  
551 simulation of big area additive manufacturing (3d printing) of a full size car, *Sampe Journal* 51 (2015) 27–36.
- 552 [23] M. Teßmann, S. Mohr, S. Gayetskyy, U. Haßler, R. Hanke, G. Greiner, Automatic determination of fiber-length distribution in composite  
553 material using 3d ct data, *EURASIP journal on advances in signal processing* 2010 (2010) 1–9.
- 554 [24] D. Salaberger, K. A. Kannappan, J. Kastner, J. Reussner, T. Auinger, Evaluation of computed tomography data from fibre reinforced polymers  
555 to determine fibre length distribution, *International Polymer Processing* 26 (2011) 283–291.
- 556 [25] H. Shen, S. Nutt, D. Hull, Direct observation and measurement of fiber architecture in short fiber-polymer composite foam through micro-ct  
557 imaging, *Composites science and technology* 64 (2004) 2113–2120.
- 558 [26] S.-Y. Fu, B. Lauke, Effects of fiber length and fiber orientation distributions on the tensile strength of short-fiber-reinforced polymers,  
559 *Composites Science and Technology* 56 (1996) 1179–1190.
- 560 [27] T. Mishurova, N. Rachmatulin, P. Fontana, T. Oesch, G. Bruno, E. Radi, I. Sevostianov, Evaluation of the probability density of inhomogeneous  
561 fiber orientations by computed tomography and its application to the calculation of the effective properties of a fiber-reinforced composite,  
562 *International Journal of Engineering Science* 122 (2018) 14–29.
- 563 [28] S. K. Kugler, A. P. Dey, S. Saad, C. Cruz, A. Kech, T. Osswald, A flow-dependent fiber orientation model, *Journal of Composites Science* 4  
564 (2020) 96.
- 565 [29] G. D. Goh, Y. L. Yap, S. Agarwala, W. Y. Yeong, Recent progress in additive manufacturing of fiber reinforced polymer composite, *Advanced*  
566 *Materials Technologies* 4 (2019) 1800271.
- 567 [30] S. Ding, B. Zou, P. Wang, H. Ding, Effects of nozzle temperature and building orientation on mechanical properties and microstructure of  
568 peck and pei printed by 3d-fdm, *Polymer Testing* 78 (2019) 105948.
- 569 [31] F. Ning, W. Cong, J. Qiu, J. Wei, S. Wang, Additive manufacturing of carbon fiber reinforced thermoplastic composites using fused deposition  
570 modeling, *Composites Part B: Engineering* 80 (2015) 369–378.
- 571 [32] C. Meola, C. Toscano, Flash thermography to evaluate porosity in carbon fiber reinforced polymer (cfrps), *Materials* 7 (2014) 1483–1501.
- 572 [33] T. Mulholland, S. Goris, J. Boxleitner, T. A. Osswald, N. Rudolph, Process-induced fiber orientation in fused filament fabrication, *Journal of*  
573 *Composites Science* 2 (2018) 45.
- 574 [34] S. Yu, Y. H. Hwang, J. Y. Hwang, S. H. Hong, Analytical study on the 3d-printed structure and mechanical properties of basalt fiber-reinforced  
575 pla composites using x-ray microscopy, *Composites Science and Technology* 175 (2019) 18–27.
- 576 [35] A. Badran, D. Marshall, Z. Legault, R. Makovetsky, B. Provencher, N. Piché, M. Marsh, Automated segmentation of computed tomography  
577 images of fiber-reinforced composites by deep learning, *Journal of Materials Science* 55 (2020) 16273–16289.
- 578 [36] J. M. Sietins, J. C. Sun, D. B. K. Jr, Fiber orientation quantification utilizing x-ray micro-computed tomography, *Journal of Composite*  
579 *Materials* 55 (2021) 1109–1118.
- 580 [37] M. P. Starmans, S. R. van der Voort, J. M. C. Tovar, J. F. Veenland, S. Klein, W. J. Niessen, Radiomics: Data mining using quantitative medical  
581 image features, in: *Handbook of medical image computing and computer assisted intervention*, Elsevier, 2020, pp. 429–456.



- 582 [38] R. F. Agyei, M. D. Sangid, A supervised iterative approach to 3d microstructure reconstruction from acquired tomographic data of  
583 heterogeneous fibrous systems, *Composite Structures* 206 (2018) 234–246.
- 584 [39] T. Baranowski, D. Dobrovolskij, K. Dremel, A. Hölzing, G. Lohfink, K. Schladitz, S. Zabler, Local fiber orientation from x-ray region-of-  
585 interest computed tomography of large fiber reinforced composite components, *Composites Science and Technology* 183 (2019) 107786.
- 586 [40] J. P. Chiverton, A. Kao, M. Roldo, G. Tozzi, Automatic diameter and orientation distribution determination of fibrous materials in micro x-ray  
587 ct imaging data, *Journal of microscopy* 272 (2018) 180–195.
- 588 [41] P. A. Hessman, T. Riedel, F. Welschinger, K. Hornberger, T. Böhlke, Microstructural analysis of short glass fiber reinforced thermoplastics  
589 based on x-ray micro-computed tomography, *Composites Science and Technology* 183 (2019) 107752.
- 590 [42] F. Chen, Y. Chen, H. D. Tagare, A new framework of multiphase segmentation and its application to partial volume segmentation, *Applied*  
591 *Computational Intelligence and Soft Computing* 2011 (2011).
- 592 [43] S. Evsevlev, S. Paciornik, G. Bruno, Advanced deep learning-based 3d microstructural characterization of multiphase metal matrix  
593 composites, *Advanced Engineering Materials* 22 (2020) 1901197.
- 594 [44] R. Lorenzoni, I. Curosu, S. Paciornik, V. Mechtcherine, M. Oppermann, F. Silva, Semantic segmentation of the micro-structure of  
595 strain-hardening cement-based composites (shcc) by applying deep learning on micro-computed tomography scans, *Cement and Concrete*  
596 *Composites* 108 (2020) 103551.
- 597 [45] C. Aguilar, I. A. Hanhan, R. F. Agyei, M. D. Sangid, M. Comer, Void detection and fiber extraction for statistical characterization of fiber-  
598 reinforced polymers, *Electronic Imaging* 2020 (2020) 250–1.
- 599 [46] T. Li, M. Comer, J. Zerubia, A connected-tube mpp model for object detection with application to materials and remotely-sensed images, in:  
600 2018 25th IEEE International Conference on Image Processing (ICIP), IEEE, 2018, pp. 1323–1327.
- 601 [47] C. Aguilar, M. Comer, A marked point process model incorporating active contours boundary energy, *Electronic Imaging* 2018 (2018) 230–1.
- 602 [48] B. Mlekusch, E. Lehner, W. Geymayer, Fibre orientation in short-fibre-reinforced thermoplastics i. contrast enhancement for image analysis,  
603 *Composites science and technology* 59 (1999) 543–545.
- 604 [49] S. Goris, T. A. Osswald, Fiber orientation measurements using a novel image processing algorithm for micro-computed tomography scans,  
605 in: *Proceedings of Society of Plastics Engineers, 15th Annual Automotive Composites Conference and Exhibition*, 2015.
- 606 [50] Y. Sinchuk, P. Kibleur, J. Aelterman, M. N. Boone, W. Van Paepegem, Variational and deep learning segmentation of very-low-contrast x-ray  
607 computed tomography images of carbon/epoxy woven composites, *Materials* 13 (2020) 936.
- 608 [51] M. W. Czabaj, M. L. Riccio, W. W. Whitacre, Numerical reconstruction of graphite/epoxy composite microstructure based on sub-micron  
609 resolution x-ray computed tomography, *Composites Science and Technology* 105 (2014) 174–182.
- 610 [52] P. J. Creveling, W. W. Whitacre, M. W. Czabaj, A fiber-segmentation algorithm for composites imaged using x-ray microtomography:  
611 Development and validation, *Composites Part A: Applied Science and Manufacturing* 126 (2019) 105606.
- 612 [53] M. J. Emerson, K. M. Jespersen, A. B. Dahl, K. Conradsen, L. P. Mikkelsen, Individual fibre segmentation from 3d x-ray computed tomography  
613 for characterising the fibre orientation in unidirectional composite materials, *Composites Part A: Applied Science and Manufacturing* 97 (2017)  
614 83–92.
- 615 [54] M. J. Emerson, V. A. Dahl, K. Conradsen, L. P. Mikkelsen, A. B. Dahl, Statistical validation of individual fibre segmentation from tomograms  
616 and microscopy, *Composites Science and Technology* 160 (2018) 208–215.
- 617 [55] V. A. Dahl, M. J. Emerson, C. H. Trinderup, A. B. Dahl, Content-based propagation of user markings for interactive segmentation of patterned  
618 images, in: *Proceedings of the IEEE/CVF Conference on Computer Vision and Pattern Recognition Workshops*, 2020, pp. 994–995.

- 619 [56] K. Kamnitsas, C. Ledig, V. F. Newcombe, J. P. Simpson, A. D. Kane, D. K. Menon, D. Rueckert, B. Glocker, Efficient multi-scale 3d cnn with  
620 fully connected crf for accurate brain lesion segmentation, *Medical image analysis* 36 (2017) 61–78.
- 621 [57] A. Prason, K. Petersen, C. Igel, F. Lauze, E. Dam, M. Nielsen, Deep feature learning for knee cartilage segmentation using a triplanar  
622 convolutional neural network, in: *International conference on medical image computing and computer-assisted intervention*, Springer, 2013,  
623 pp. 246–253.
- 624 [58] W. Whitacre, M. Czabaj, Automated 3d digital reconstruction of fiber reinforced polymer composites, in: *AIAA Guidance, Navigation, and  
625 Control Conference*, 2015, p. 0342.
- 626 [59] H. Altendorf, 3D Morphological analysis and modeling of random fiber networks: applied on glass fiber reinforced composites, Ph.D. thesis,  
627 Paris, ENMP, 2011.
- 628 [60] K. Breuer, M. Stommel, Rve modelling of short fiber reinforced thermoplastics with discrete fiber orientation and fiber length distribution,  
629 *SN applied Sciences* 2 (2020) 1–13.
- 630 [61] L. Wang, G. Nygren, R. L. Karkkainen, Q. Yang, A multiscale approach for virtual testing of highly aligned short carbon fiber composites,  
631 *Composite Structures* 230 (2019) 111462.
- 632 [62] M. J. Emerson, K. M. Jespersen, Y. Wang, P. J. Withers, V. A. Dahl, K. Conradsen, L. P. Mikkelsen, A. B. Dahl, Insegt fibre: A powerful  
633 segmentation tool for quantifying fibre architecture in composites, in: *Int. Conf. Tomography of Materials & Structures*. Cairns, Australia,  
634 2019.
- 635 [63] A. Nasirov, I. Fidan, Prediction of mechanical properties of fused filament fabricated structures via asymptotic homogenization, *Mechanics  
636 of Materials* 145 (2020) 103372.
- 637 [64] S. Wilkins, T. E. Gureyev, D. Gao, A. Pogany, A. Stevenson, Phase-contrast imaging using polychromatic hard x-rays, *Nature* 384 (1996)  
638 335–338.
- 639 [65] S. Van der Walt, J. L. Schönberger, J. Nunez-Iglesias, F. Boulogne, J. D. Warner, N. Yager, E. Gouillart, T. Yu, scikit-image: image processing  
640 in python, *PeerJ* 2 (2014) e453.
- 641 [66] S. R. Biswal, T. Sahoo, S. Sahoo, Prediction of grain boundary of a composite microstructure using digital image processing: A comparative  
642 study, *Materials Today: Proceedings* 41 (2021) 357–362.
- 643 [67] P. Virtanen, R. Gommers, T. E. Oliphant, M. Haberland, T. Reddy, D. Cournapeau, E. Burovski, P. Peterson, W. Weckesser, J. Bright, S. J.  
644 van der Walt, M. Brett, J. Wilson, K. J. Millman, N. Mayorov, A. R. J. Nelson, E. Jones, R. Kern, E. Larson, C. J. Carey, Í. Polat, Y. Feng,  
645 E. W. Moore, J. VanderPlas, D. Laxalde, J. Perktold, R. Cimrman, I. Henriksen, E. A. Quintero, C. R. Harris, A. M. Archibald, A. H. Ribeiro,  
646 F. Pedregosa, P. van Mulbregt, SciPy 1.0 Contributors, SciPy 1.0: Fundamental Algorithms for Scientific Computing in Python, *Nature  
647 Methods* 17 (2020) 261–272.
- 648 [68] The opencv reference manual: Image segmentation with watershed algorithm, 2014. URL: [https://docs.opencv.org/4.x/d3/db4/  
649 tutorial\\_py\\_watershed.html](https://docs.opencv.org/4.x/d3/db4/tutorial_py_watershed.html).