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Thermal properties of methyltrimethoxysilane aerogel thin films

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Aerogels are light and porous solids whose properties, largely determined by their nanostructure, are useful in a wide range of applications, e.g., thermal insulation. In this work, as-deposited and thermally treated air-filled silica aerogel thin films synthesized using the sol-gel method were studied for their thermal properties using the 3-omega technique, at ambient conditions. The thermal conductivity and diffusivity were found to increase as the porosity of the aerogel decreased. Thermally treated films show a clear reduction in thermal conductivity compared with that of as-deposited films, likely due to an increase of porosity. The smallest thermal conductivity and diffusivity found for our aerogels were $0.019 \text{ W m}^{-1} \text{ K}^{-1}$ and $9.8 \times 10^{-9} \text{ m}^2 \text{ s}^{-1}$. A model was used to identify the components (solid, gaseous and radiative) of the total thermal conductivity of the aerogel. © 2016 Author(s). All article content, except where otherwise noted, is licensed under a Creative Commons Attribution (CC BY) license (<http://creativecommons.org/licenses/by/4.0/>). [<http://dx.doi.org/10.1063/1.4965921>]

I. INTRODUCTION

Silica aerogels exhibit low density ($\approx 100 \text{ kg m}^{-3}$), porosity between 80% and 99.8%, pore sizes in the range of nanometers ($\approx 15 \text{ nm}$), high specific surface area ($\approx 1000 \text{ m}^2 \text{ g}^{-1}$), very low thermal conductivity ($\approx 0.01 \text{ W m}^{-1} \text{ K}^{-1}$), optical transparency in the visible spectrum ($\approx 85\%$), low refractive index (1.05) and superhydrophobicity.^{1,2} Their properties have attracted attention due to their wide range of applications, such as in thermal and acoustic insulation,¹ kinetic energy absorption,³ fiber optics⁴ and antireflection coatings.⁵

Silica aerogels can be easily synthesized in monoliths, grains, powders and films via sol-gel,^{2,6} using common precursors such as tetramethyl orthosilicate (TMOS) and tetraethyl orthosilicate (TEOS), following a critical point drying process. To reduce costs and synthesis complexity, aerogels have been fabricated in ambient conditions using, for instance, TEOS with a silylation process⁷⁻⁹ or a dedicated precursor such as methyltrimethoxysilane (MTMS).^{5,10,11} Both methods produce aerogels covered with methyl groups, providing hydrophobic behavior which prevents the possible collapse of the aerogel that might occur upon drying. Silylation is based on the introduction of silyl groups in the aerogel surface before drying, while MTMS precursors yield aerogels in ambient conditions without any modification, since their molecular structure¹¹ (Fig. S1 in the [supplementary material](#)), including methyl groups, provides hydrophobicity^{5,10} and mechanical flexibility¹² to the aerogel. The 3-omega method has been used extensively for measuring the thermal conductivity and diffusivity of isotropic and anisotropic thin films, bulk materials,¹³ porous films^{7,14,15} and multilayer stacks.^{16,17}

Here, we report on the thermal conductivity and diffusivity of MTMS-based aerogels obtained using the 3-omega method in ambient conditions. Based on their compatibility, different percentages

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of TEOS and TMOS (as co-precursors) were mixed with MTMS, to explore the possibility of controlling the structural, optical and thermal properties of the aerogel. Finally, a thermal conductivity vs. density model was used to describe the contribution of the solid particles, the gas inside the pores and the radiative components of the aerogel to the total thermal conductivity.

II. EXPERIMENTAL DETAILS

The fabrication of silica aerogel films was carried out in a two-step sol-gel procedure. All chemicals were purchased from Sigma-Aldrich and used as received. The main precursor for the aerogel syntheses was MTMS, with TMOS or TEOS as co-precursors. Syntheses were performed at room temperature and pressure using the following procedure:^{5,10,18} $(0.5 - x)$ mL MTMS + x mL TMOS or TEOS (where $x = 0, 5, 12.5, 25, 37.5, 50$ μ L for TMOS, and $x = 0, 50, 100, 150$ μ L for TEOS, giving a total volume of 0.5 mL + 4.87 mL of MeOH + 0.25 mL of 10 mM oxalic acid were dissolved and stirred for 30 min, then left to rest for hydrolysis during 24 h. Then, 0.31 mL of 11.2 M NH_4OH (aq) was added and the new solution, stirred for 15 min, was sealed to prevent evaporation and for condensation and aging for 48 h. The result was a gel with alcohol-filled pores (alcogel).¹ After addition of MeOH the alcogel was sonicated at 20 kHz, to obtain a homogenized solution. Then, films were obtained by spin-coating the homogenized solutions on thermally grown SiO_2 substrates at 2000 rpm for 40 s, providing complete substrate coverage and negligible edge effects (Fig. S2 in the [supplementary material](#)). The effect of thermal treatment was also studied by thermally drying the aerogel films at 450 °C for 1 h after deposition.

Structural analysis of the aerogels was performed using an ESEM Quanta 200 FEG Scanning Electron Microscope (SEM), a white light optical profiler Fogale Nanotech Photomap 3D and a Veeco Dektak 150 profilometer. Optical characterization was carried out using a variable angle spectroscopic ellipsometer RC2 (from 190 nm to 1700 nm) and an infrared spectrometer from J. A. Woollam Co. Inc.

The 3-omega method was set up to determine the thermal properties of the aerogel films.^{13,19–21} Conventional lithography was used to pattern the top contact pads. A 200 nm thick SiO_2 capping layer was sputtered, using an RF magnetron sputtering tool. This avoided penetration of the pores.⁷ Then, Au was deposited by e-beam evaporation to produce the metal contacts for heating and thermometry⁷ (Fig. S3 in the [supplementary material](#)). The driving current was supplied by a Keithley 6221 AC source. First (1ω) and third (3ω) harmonic voltages frequency responses were detected with lock-in Signal Recovery 7265. The thermal coefficient of resistance (c_{tr}) was determined from the resistance-temperature evolution, obtained by setting a temperature ramp with a Peltier stage between 15 °C and 60 °C and recording the 4-point probe resistance with an Agilent 3458a digital multimeter.

III. RESULTS AND DISCUSSIONS

The behavior of the film porosity, thickness and roughness for different TMOS v/v%²² in the synthesis was investigated first (Fig. 1). A comparison of the thicknesses obtained with profilometry and ellipsometry is presented in Fig. S4(a) in the [supplementary material](#). The porosity and the refractive index values of the aerogels were calculated from ellipsometry spectra using the effective medium theory considering the aerogel as a composite of air and silica.^{5,10,23,24} The porosity was obtained using the relation $(1.399 - n_{\text{aerogel}})/(1.399 - n_{\text{air}})$, where n_{aerogel} and n_{air} are the refractive indexes of the aerogel (Fig. 1(a)) and air, respectively, and 1.399 indicates the refractive index of the non-porous aerogel.⁵

It was found that the higher the TMOS v/v% the lower the porosity, whereas the thickness shows its minimum value at 5 v/v%, and a maximum at 0 v/v% TMOS (Fig. 1(b)). The root mean squared (RMS) roughness of the films was found to decrease as the TMOS v/v% increased, with a quasi-plateau for TMOS v/v% values higher than 5% (Fig. 1(c)). This behavior of the roughness parameter is in agreement with that of the porosity, considering that lower porosities induce lower roughness.²⁵ For aerogels synthesized with TEOS, the porosity shows similar trends. The thickness decreases as the TEOS percentage increases, and the roughness

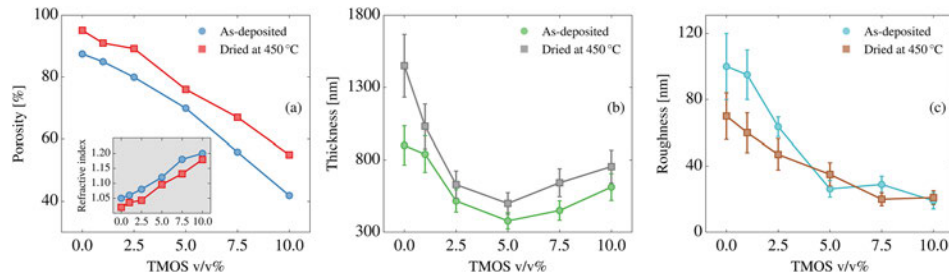


FIG. 1. (a) Porosity, (b) thickness, and (c) RMS roughness of as-deposited and thermally treated aerogel films fabricated with MTMS and different TMOS v/v%. Inset of (a): refractive index (at $\lambda = 550$ nm) vs. TMOS v/v%. Lines are visual guides.

stabilizes, after a considerable drop, when TEOS reaches 20 v/v% (Figs. S4(b) and S5 in the [supplementary material](#)). SEM images confirmed smoother aerogel surfaces in the presence of TMOS (Fig. 2).^{5,7,10,18,26,27}

A set of aerogel films was thermally treated after deposition to study the effects of this process on the thermal properties of the films. First, an optimization was performed to determine the optimal temperature for the thermal treatment. Three similar aerogel samples were dried at 200 °C, 300 °C and 450 °C, where the best performance was found at 450 °C, in agreement with other works.^{5,7–10} Thermally treated samples at 450 °C show higher porosity and thickness, as well as smoother surfaces (Fig. 1). The increase of the thickness can be explained in terms of the spring-back effect taking place in the aerogels after the initial shrinkage associated with the drying process.^{5,7–10}

FTIR spectra were measured to determine the chemical composition of the aerogels with different percentages of TMOS and TEOS. One of the advantages of using the MTMS precursor is the presence of the non-hydrolyzable methyl groups on the aerogel surface^{5,10} (Fig. 3). These groups make the aerogels hydrophobic and, thus, prevent their collapse upon drying. As the TMOS v/v% is increased, the Si–CH₃ contributions at 790 cm^{−1} (rocking mode) and 1275 cm^{−1} (symmetrical deformation mode) decrease^{26,28,29} and films become more hydrophilic.^{5,10} An analogous effect is observed with TEOS precursor (Fig. S6 in the [supplementary material](#)).

The thermal properties of the aerogel films were characterized using the 3-omega technique. The transformations of the measured 1ω and 3ω voltages into temperature spectra were performed taking into account the half-width (b) and length (l) of the Au line, and the thermal coefficient of resistance (c_{tr}).³⁰ The thermal conductivity and diffusivity were then obtained by fitting the measured temperature spectra with the heat-conduction model for thin film multilayers developed by Borca-Tasciuc, assuming the aerogel films act as isotropic materials. Including heat conduction effects inside the heater, the heater's temperature rise is given by:¹³

$$T_{h,2\omega} = \frac{T_{2\omega}}{1 + i 4 \omega (\rho_h c_h d_h) \left(\frac{b l}{p} \right) T_{2\omega}} \quad (1)$$

where $T_{2\omega}$ is the temperature change without taking into account heater effects, p is the peak electrical power, ω is the angular frequency, $(\rho_h c_h)$ and d_h , the heat capacitance and thickness of the heater.

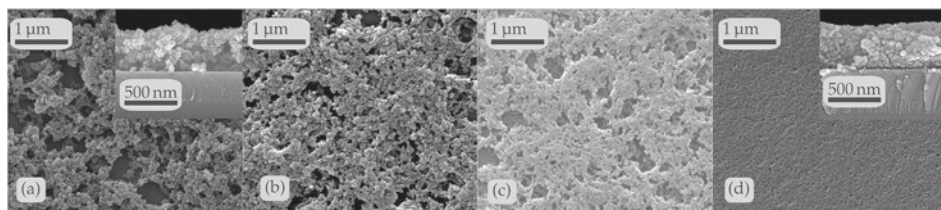


FIG. 2. SEM images of as-deposited aerogels: (a) 100 v/v% MTMS aerogel; inset: cross-section of the aerogel film; (b) Aerogel with 2.5 v/v% TMOS; (c) Aerogel with 5 v/v% TMOS; (d) Aerogel with 10 v/v% TMOS; inset: cross-section of the aerogel film.

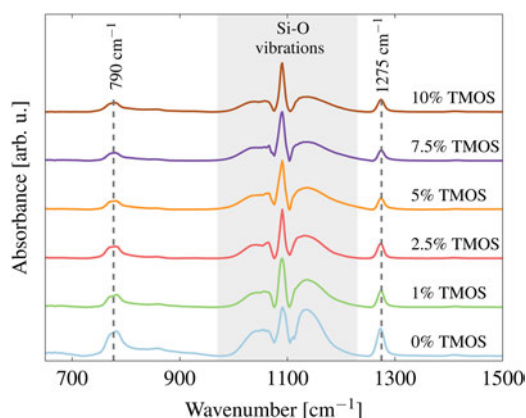


FIG. 3. Absorbance FTIR spectra of the MTMS aerogel films synthesized with different TMOS v/v%. The shaded area around 1100 cm^{-1} shows typical Si-O contributions in silica aerogels, while bands at 790 cm^{-1} and 1275 cm^{-1} are associated to the Si-CH₃ related modes.

The setup was validated (Figs. S7–S9 in the [supplementary material](#)). In order to characterize each aerogel film, a four-layer system was configured: sputtered SiO₂ ($\approx 200\text{ nm}$ thick)/aerogel film/thermal SiO₂ ($\approx 200\text{ nm}$ thick)/Si wafer ($525\text{ }\mu\text{m}$ thick). The thermal conductivity and diffusivity of thermal and sputtered SiO₂ layers, as determined with the 3-omega setup, were $1.499\text{ W m}^{-1}\text{ K}^{-1}$ and $7.59 \times 10^{-7}\text{ m}^2\text{ s}^{-1}$, for the thermal SiO₂, and $1.024\text{ W m}^{-1}\text{ K}^{-1}$ and $6.70 \times 10^{-7}\text{ m}^2\text{ s}^{-1}$ for the sputtered SiO₂, in agreement with previous works.^{31–34} The silicon wafer's parameters were taken from literature.³⁵ The thermal conductivity and diffusivity of the MTMS aerogel were obtained using the Borca-Tasciuc model for different TMOS v/v% (Fig. 4). Temperature-frequency spectra show excellent agreement with theoretical fits (Fig. S7 in the [supplementary material](#)). It was found that the higher the TMOS v/v% the larger is the thermal conductivity, attributable to the decrease of porosity. The thermal diffusivity ranges between 10^{-8} – $10^{-7}\text{ m}^2\text{ s}^{-1}$. Similar behavior was found for aerogels based on TEOS (Fig. S10 in the [supplementary material](#)).

The thermal conductivity and diffusivity of thermally treated aerogels increase as the porosity decreases, following the same tendency of non-treated samples. However, the thermal treatment reduces the thermal conductivity with the lowest value observed being $0.019\text{ W m}^{-1}\text{ K}^{-1}$ (Fig. 4(a)). This is 20% lower than that of air at standard conditions of temperature and pressure ($0.026\text{ W m}^{-1}\text{ K}^{-1}$).³⁶ Furthermore, it is one of the lowest thermal conductivity values for non-silylated and air-filled (non-evacuated) MTMS-based aerogel films, synthesized at ambient conditions.^{1,7,8} The thermal diffusivity also decreases after thermal treatment (Fig. 4(b)).

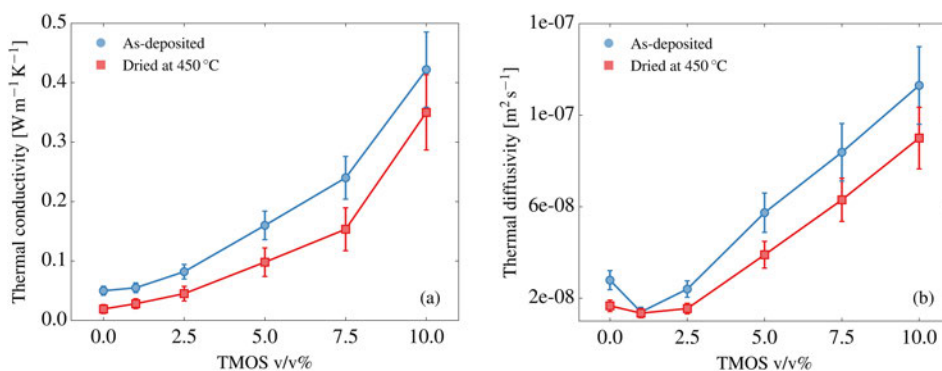


FIG. 4. Thermal conductivity (a) and diffusivity (b) of as-deposited and thermally treated MTMS aerogel films fabricated with different TMOS v/v%. Lines are visual guides.

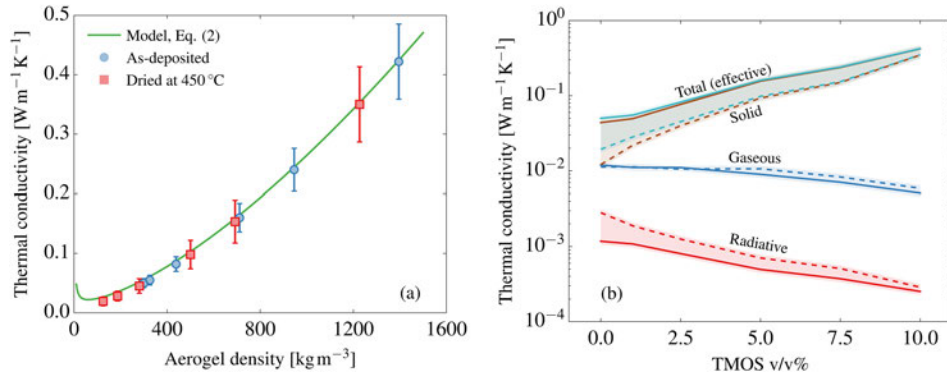


FIG. 5. (a) Thermal conductivity vs density evolution of the as-deposited and thermally dried MTMS aerogel films fabricated with different TMOS v/v%. The continuous line represents the model (Eqs. (2)). (b) Contributions of the solid (Eq. (2a)), gas (Eq. (2b)) and radiative (Eq. (2c)) phases to the total thermal conductivity. Continuous lines correspond to the as deposited samples and dashed lines to thermally treated samples.

The thermal conductivity of non-evacuated aerogels can be described by the conduction through the small solid particles, k_s , and the gas inside the pores, k_g , and the radiation, k_r :³⁷

$$k_s = \rho_{\text{aerogel}} v_{\text{aerogel}} [k_{\text{SiO}_2} / \rho_{\text{SiO}_2} v_{\text{SiO}_2}] \quad (2a)$$

$$k_g = (k_{g,0} \Pi) / (1 + 2 K_n) \quad (2b)$$

$$k_r = (16 n^2 \sigma T^3) / (3 \rho_{\text{aerogel}} \kappa_{\text{SiO}_2} / \rho_{\text{SiO}_2}) \quad (2c)$$

where k_{SiO_2} , ρ_{SiO_2} , v_{SiO_2} and κ_{SiO_2} denote the thermal conductivity, the density, the sound velocity and the extinction coefficient of silica, respectively, Π , n and ρ_{aerogel} are the porosity, effective refractive index, density and the sound velocity of the aerogel, respectively, $k_{g,0}$ the thermal conductivity of still free air at standard conditions of pressure and temperature, K_n the Knudsen number, σ the Boltzmann constant, and T the temperature inside the material. Taking the porosity and the refractive index of the aerogels from Fig. 1, and the other parameters indicated in Eqs. (2) from the literature^{37–39} ($v_s = 5900 \text{ ms}^{-1}$, $p_s = 2200 \text{ kg m}^{-3}$, $k_s = 1.34 \text{ W m}^{-1} \text{ K}^{-1}$, $k_{g,0} = 0.026 \text{ W m}^{-1} \text{ K}^{-1}$, $\alpha = 2$, $n = 1$, $\sigma = 5.67 \times 10^{-8} \text{ W m}^{-2} \text{ K}^{-4}$, $K_s = 22.7$), the relationship between thermal conductivity and density was plotted, both for the as-deposited and the thermally dried aerogels (Fig. 5(a)). The smallest density value obtained was 110 kg m^{-3} , for a thermally dried aerogel with 0 v/v% TMOS. In the low density region, the thermal conductivity exhibited a slight deviation from the model, attributable to limited validity of the model assumptions and the hypothesis that the aerogel is exclusively made of silica. The contributions to the thermal conductivity were calculated from Eqs. (2), and are shown in Fig. 5(b). The largest contribution to the thermal conductivity comes from the solid phase (silica particles); this contribution significantly decreases after thermal treatment as a consequence of the lower density. The gaseous phase contribution is one order of magnitude smaller than that of the solid phase. The thermal treatment of the aerogels has a negligible effect on the gas phase contribution. The radiative component, as a consequence of the low mass fraction and the large surface area of silica aerogels,³⁷ together with the fact that experiments were performed at room temperature (Eqs. (2)), has a negligible contribution. An increase of the radiative contribution is observed for samples thermally dried after deposition, probably due to the smaller values of the density. Smaller particle sizes decrease the radiative component by raising the complexity of the solid path in the aerogel network, reducing the gas flow and creating a larger number of interfaces that act as barriers to the propagation of thermal radiation.⁴⁰ The same analysis on aerogel films including TEOS shows a similar behavior (Figs. S11 and S12 in the [supplementary material](#)). Particle size were estimated from SEM images for the TMOS precursor aerogels at 0, 2.5, 5 and 10 v/v%, yielding about 28.9, 33, 44 and 53 nm for the as-deposited aerogels, and about 16, 30, 23 and 41 nm for the thermally treated ones, respectively. As expected from the thermal conductivity behavior of the aerogels, it is possible to conclude the smaller particle sizes induce a decrease in the porosity.^{16,40–42}

IV. CONCLUSIONS

Aerogel thin films based on MTMS were synthesized and their functional properties investigated at standard temperature and pressure conditions. The structural optical and thermal properties of the aerogels were modified by inclusion of TMOS and TEOS as co-precursors during synthesis.

The porosity and roughness of the films were found to decrease with the increase of the v/v% of TMOS and TEOS, whereas the film thickness shows a minimum for 5 v/v% TMOS, and decreases monotonically for TEOS. Significant increases in the porosity (up to 8%) and thickness (up to 50%) were observed for thermally treated films. The increase in the thickness was attributed to an enhanced spring-back effect, inducing greater porosity.

The thermal conductivity of the aerogels was found to increase quasi-linearly with the co-precursor v/v%. This is probably associated with the porosity since higher porosity implies lower conductivity. The same trend was observed for the thermal diffusivity of the films. Films after thermal treatment exhibited lower thermal conductivity and diffusivity compared with those of the as-deposited films: the smallest values reached for non-evacuated and non-silylated aerogels were $0.019 \text{ W m}^{-1} \text{ K}^{-1}$ (20% lower than that of air at standard conditions of temperature and pressure, $0.026 \text{ W m}^{-1} \text{ K}^{-1}$) and $9.8 \times 10^{-9} \text{ m}^2 \text{ s}^{-1}$, respectively.

Employing a simple density model, the solid, gaseous and radiative thermal contributions to the total thermal conductivity of the aerogels were studied. The solid phase contribution is greatest, one order of magnitude more than that of the gaseous phase. The radiative contribution was found to be negligible. Particle size were found to increase with larger amounts of TMOS v/v% in the mixture. It can also be stated that the lowest values of thermal conductivity are observed for aerogels with the smaller particle sizes. Work is in progress to deduce the particle sizes in TEOS aerogels and the results will be object of a further publication. A thorough understanding of the effect of nanostructure sizes and features, such as inter-particle contacts, could be studied by analyzing the behavior of thermal conductivity over a wide range of pressures and temperatures, where effects such as solid-gas coupling can be used to reveal the structure of the material.^{1,41,43,44}

SUPPLEMENTARY MATERIAL

See the [supplementary material](#) for further details about the molecular structure of MTMS, aerogel homogenized solutions, 3ω setup and validation, and results for TEOS co-precursor.

ACKNOWLEDGMENTS

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