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The kinematic preshaping of triggered self-adaptive linkage-driven robotic fingers

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Abstract. In this paper, the issue of the kinematic – as opposed to dynamic – preshaping of self-adaptive robotic fingers driven by linkages is discussed. A method to obtain designs of these fingers capable of various behaviours during their closing motions is presented. The method is based on using triggered passive elements in carefully selected joints of the finger and the selection or optimization of geometric parameters to obtain particular kinematic relationships between the motions of the phalanges. This method is very general and can be applied to any self-adaptive robotic finger in order to obtain many different types of closing motions. Examples given in this paper are focusing on two different preshaping motions, the first one aims at allowing pinch grasps while the second mimics a human finger. The fundamental aim of this paper is to show that various preshapings of self-adaptive fingers are possible, not just one, and to give two step-by-step examples.

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1 Introduction

1.1 Self-adaptive fing rs

In the past few years, a significant increase in the development of innovative technologies has tried to address the lack of commercial success of complex robotic hands. Significant efforts have been made to find designs simple enough to be easily built and controlled (Bicchi, 2000), particularly in human prosthetics. A special emphasis has been placed on the reduction of the number of degrees of freedom (DOF), thereby decreasing the number of required actuators. In particular, the SSL hand (Akin et al., 2002), the DIES-DIEM hand (Biagiotti et al., 2001) and the Cassino finger (Figliolini and Ceccarelli, 2002) have followed this path. On the other hand, a rapidly growing number of prototypes involve a smaller number of actuators without decreasing the number of DOF by taking advantages of self-adaptive, a.k.a. underactuated, mechanisms. These prototypes are usually either driven by tendons (Hirose and Umetani, 1978; Crisman et al., 1996; Massa et al., 2002; Higashimori et al., 2005a) or by linkages (Bekey et al., 1999; Ulrich, 1988; Laliberté and Gosselin, 1998; Kennedy, 2001; Ceccarelli et al., 2006b). This approach leads to the automatic/mechanical adaptation of the robotic finger to the shape of the object seized. A classic example of a self-adaptive two-DOF finger driven by linkages and its closing sequence is illustrated in Fig. 1.

Self-adaptive mechanisms offer tremendous possibilities and have been known for decades but they have been kept in the shadows of the exponentially growing capability of digital architectures. These mechanical systems have been superseded by their electronic counterpart which provided better, more accurate, cheaper and faster means of performing computing tasks (Gosselin, 2006). However, the confinement of mechanical systems to the execution of motion under the control of a higher-level controller has to be considered as a design choice rather than an obligation. In this paper:

- the kinematic preshaping of self-adaptive fingers is defined,
- two examples are given: pinch and anthropomorphic with the two-phalanx class S finger,
- geometric parameters to achieve these preshapings are either selected or optimized,
- limitations and extensions of the proposed methodology are discussed.

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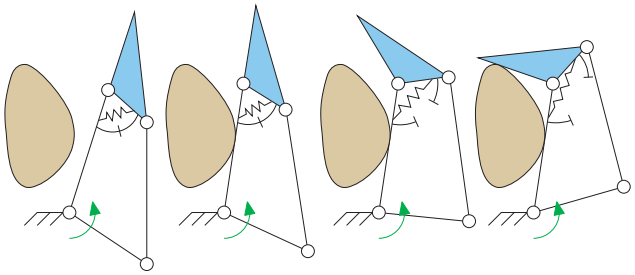

Figure 1. Closing sequence of a two-DOF self-adaptive finger.

2 Kinematics of triggered self-adaptive fingers

2.1 Introduction

The essence of self-adaptive fingers is twofold: a transmission linkage used to transmit actuation to the phalanges, and passive elements used to constrain the finger. In this paper, it is assumed that the finger is driven by a single actuator and unless otherwise specified the latter is located between the ground and the transmission linkage. Passive elements, as illustrated in Fig. 1, are key to prevent any undesired motions of the finger since the latter has n-DOF while having as few as one actuator. It is the aim of this paper to present how, by carefully selecting the type and location of these passive elements, several very interesting behaviours can be achieved. Many different types of passive elements may be considered (Birglen, 2009). Each of them applies a constraint (i.e. *a torque/force*) to a selected joint in the linkage. Springs and triggered springs are by far the most popular choice to achieve this goal. Using a triggered element in one of the joints of a self-adaptive finger, one locks this joint when no external constraint if applied to the mechanism, i.e. when no contact has yet occurred. Therefore, with a n-phalanx self-adaptive finger when $n-1$ triggered elements are used, one obtains a single DOF linkage. If a reasonable number (e.g. less than 6) of binary/ternary links is considered, the only possible one-DOF linkages (Birglen, 2009) are the four-bar, Watt's and Stephenson's linkages, illustrated in Fig. 2.

Hence, when no external contact has yet occurred, the self-adaptive finger considered behaves as one of these three linkages. Therefore, if triggered elements are used, a purely kinematic relationship exists between the angles of the phalanges θ_i and actuation, i.e. one has

$$g_i(\theta_i,\theta_a)=0 \quad \text{with} \quad i=1,\ldots,n \tag{1}$$

with a n-phalanx finger where θ_a is the angle associated with actuation. A trivial case occurs when the triggered element(s) is (are) located between the phalanges j and $j-1$ or between the ground and the proximal phalanx. Both cases respectively yields $\theta_j = K$ or $\theta_1 = L$ where K and L are constants. If a triggered element is located elsewhere in the mechanism, i.e. in the transmission linkage, the functions g_i can be

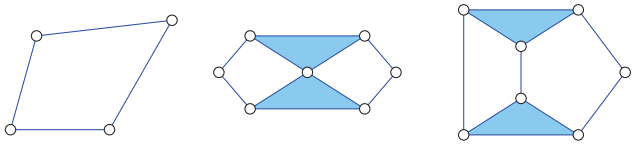

Figure 2. Four-bar, Watt's and Stephenson's one-DOF linkages.

obtained by writing the loop-closure equations of the linkage and a relationship $h(\theta_1,\ldots,\theta_n)$ can be obtained. With Watt's and Stephenson's linkages, this might be challenging as these equations are highly nonlinear and closed-form solutions have not been reported in the literature to the best of the author's knowledge (except in few cases with simplified geometries). Nevertheless, numerical values can be obtained. On the other hand, if the finger is reduced to a four-bar linkage, a closed-form solution exists. The position analysis of a four-bar linkage is actually a well-known textbook problem (Norton, 1992; McCarthy, 2000) and the relationships between the angles of the driven/driving cranks and the coupler can be obtained. Even if only the four-bar case is considered, a wide range of behaviours can be obtained as will be shown.

2.2 Kinematics of the class S

As an example, let us consider the linkage-driven two-phalanx class S finger (Birglen, 2009). A class S finger with n phalanges is constituted by a single loop linkage with $n+3$ joints. The phalanges and the ground to which they are attached are chosen as consecutive links of the mechanism and connected by revolute joints. Previously, only the case where this finger presented the particularity of having a ground link reduced to a single point was usually considered (cf. Fig. 1). This choice considerably simplifies mechanical design and the finger based on this simplification has been extensively investigated (Birglen et al., 2008). However, the more general case where two distinct joints constitute the ground link of the mechanism allows for much more freedom. It is worth mentioning that this class can be easily extended to an arbitrary number of phalanges. Indeed, the definition of this class is that the transmission mechanism is a simple planar motion generator (e.g. a RRR or RPR chain).

Triggered elements placed in any joint(s) of such a three-phalanx finger to reduce its DOF during the closing motion results in a four-bar linkage, as illustrated in Fig. 3. In this figure, the "lock" symbol has been used to indicate which joint holds the triggered element and the resulting four-bar linkage is highlighted in dashed lines. The kinematic reduction of the finger to a four-bar is true for any finger of this class when an appropriate number of triggered elements is used. A maximum number of two passive elements can be located in the joints of the transmission linkage since the latter is constituted by only three joints and the actuated joint

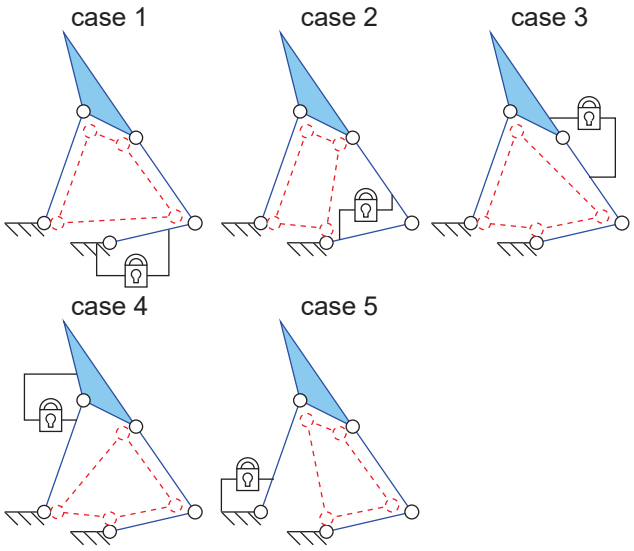

Figure 3. Kinematic reductions of the two-phalanx class S finger with one triggered element.

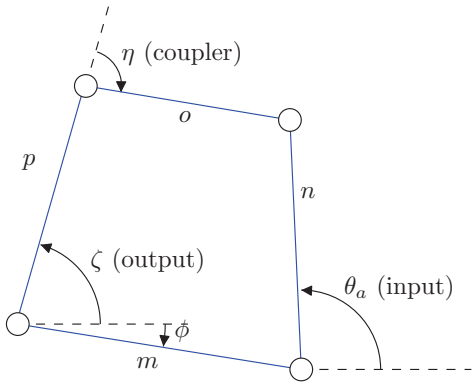

Figure 4. Modeling of a four-bar linkage.

is not a proper choice (although in certain cases it can hold a passive element, e.g. with compliant fingers). Therefore, if more passive elements are required they are necessarily located between the phalanges. Yet, the final one-DOF linkage remains a four-bar.

Let us consider the kinematic modeling of a general four-bar linkage illustrated in Fig. 4. Using the loop-closure equations, the relationships between the output/coupler, output/input and coupler/input angles are obtained. One has respectively:

$$p^2+o^2+m^2-n^2+2op\cos\eta-2mp\cos(\zeta-\phi)-2mo\cos(\phi-\zeta-\eta)=0, \quad (2)$$

$$m^2+n^2+p^2-o^2+2mn\cos(\phi-\theta_a)-2mp\cos(\phi-\zeta)-2np\cos(\theta_a-\zeta)=0, \quad (3)$$

$$m^2+n^2-o^2-p^2+2mn\cos(\theta_a-\phi)-2op\cos\eta=0. \quad (4)$$

With the two-phalanx finger and disregarding the trivial cases

Table 1. Associations of geometric parameters.

	m	n	o	p	ϕ	ζ	η
Case 1	r	b	c	l_1	$\alpha+\beta$	θ_1	$\theta_2-\psi$
Case 2	d	s	c	l_1	α	θ_1	$\theta_2-\psi$
Case 3	d	a	t	l_1	α	θ_1	$\theta_2-\psi-\gamma$

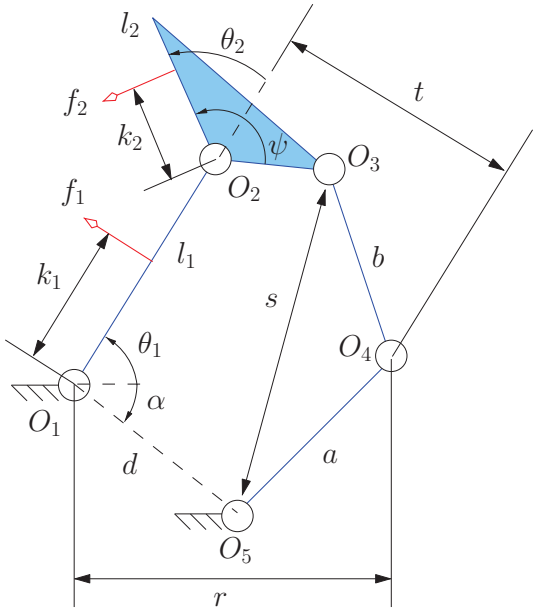

Figure 5. Details of the class S two-phalanx finger.

4 and 5, each location for the passive element yields a different association between the geometric parameters of the four-bar with these of the finger (illustrated in Fig. 5) as described in Table 1.

In this table, r is the distance between O_1 and O_4, s is the distance between O_3 and O_5 and t is the distance between O_2 and O_4. Each one of these distances is kept constant in its respective case. The angles β and γ are defined by

$$\beta=\arccos\left(\frac{r^2+d^2-a^2}{2rd}\right) \quad \text{and} \quad \gamma=\arccos\left(\frac{c^2+t^2-b^2}{2ct}\right) \quad (5)$$

Note that in case 1, actuation is assumed to be located in O_4.

Equation (2) is very important since it describes the relationship between the output phalanx angles of the mechanism directly, i.e. without θ_a. By carefully choosing the geometric parameters of the fingers and therefore the coefficients of this equation, it is possible to approximate several very interesting relationships between θ_1 and θ_2 for the finger, as will be shown.

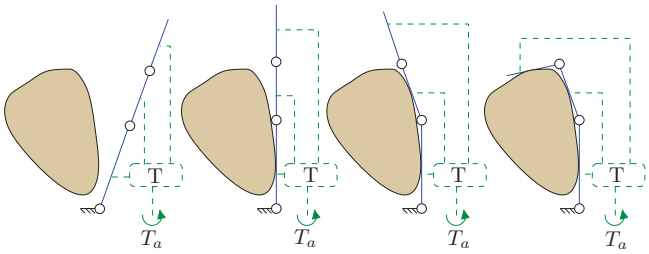

Figure 6. Closing sequence of a three-phalanx finger keeping its phalanges aligned.

3 Kinematic preshaping

3.1 Introduction and straight line preshaping

First, let us briefly recall the definition of preshaping: the preshaping of a finger – artificial or not – is defined as the set of geometric configurations this finger undertakes during the pregrasping phase, when no contact has yet occurred (Zhiwei et al., 2002; Supuk et al., 2005). With self-adaptive fingers, this issue has been overlooked in the past because of the limited set of available kinematic architectures known to be able to achieve self-adaption. Indeed, to the best of the author's knowledge, most prototypes of self-adaptive robotic fingers have springs located between their phalanges (or a kinematically equivalent design) in order for the latter to stay aligned during the pregrasping phase (as illustrated in Figs. 1 and 6). This preshaping can be done with any architectures of self-adaptive robotic finger since by definition, the phalanges are consecutive links of the mechanism and therefore, it is possible to locate spring(s) and mechanical limit(s) between them.

Recently, the Robotics Laboratory of Hiroshima University has proposed a method to optimize the preshaping of one self-adaptive robotic finger originally proposed in Hirose and Umetani (1978). This method was dealing with *dynamic preshaping* (Higashimori et al., 2005b), a particular aspect of the preshaping issue based on a dynamic analysis. Indeed, the proposed finger was subjected to very high accelerations (the authors claim to approach 100 g). With such high accelerations, dynamics becomes a critical issue and a specific dynamic preshaping, optimized to increase the probability for the finger to make contact with a spherical object using all its phalanges, was proposed based on a refined dynamic modeling. However, this method requires a thorough knowledge of the dynamics of the system which yields a significant burden to the designer and is unnecessarily complicated when low accelerations are considered. Furthermore, although this method is very accurate, results obtained are difficult to extend to other designs, for instance fingers based on linkages as in this paper.

On the other hand, *kinematic preshaping* as proposed here is defined as the preshaping of a self-adaptive finger from a quasi-static perspective, i.e. when dynamics is neglected in favor of kinematics. This approach does not require any knowledge of the dynamic of the system. Triggered elements are key to this method since they prevent motions under the assumption that dynamic forces are small. Continuous elements on the other hand are much more sensitive to these forces. Furthermore, triggered passive elements allow to consider simpler one-DOF linkages as discussed in Sect. 2 and illustrated in Fig. 2 instead of the complete mechanism. For instance, the preshaping of two-phalanx fingers such as the one described in Fig. 5 is the set of both phalanx joint angles when it is reduced to one of the linkages in Fig. 2. Disregarding again trivial cases where the triggered element is located in one of the phalanx joints, the preshaping can be described by a set of two equations, namely

$$\begin{cases} \theta_1 = g_1(\theta_a) \\ \theta_2 = g_2(\theta_a) \end{cases}. \tag{6}$$

Therefore, providing that g_1 and g_2 are invertible (at least locally), the preshaping can be described by a single equation, namely

$$g_1^{-1}(\theta_1) = g_2^{-1}(\theta_2) \Leftrightarrow h(\theta_1, \theta_2) = 0. \tag{7}$$

When the finger can be reduced to a four-bar linkage, Eq. (7) simply becomes Eq. (2). Following the same method, the preshaping of an n-phalanx finger can be described by a set of $n-1$ equations. This set of equations usually cannot match a particular desired preshaping except in some simple cases (e.g. in Sect. 3.2). However, the difference between the sets of equations describing the actual and desired preshaping can be characterized by a performance index and an optimization procedure can be used to maximize this index.

3.2 Pinch preshaping

An interesting feature of a few self-adaptive robotic fingers proposed in the literature (Gosselin and Laliberté, 1996; Bartholet, 1992; Bégoc et al., 2004) is the ability to maintain their distal phalanx perpendicular to the palm during their closing sequence. This kinematic property allows pinch grasps as illustrated in Fig. 7. This is very useful when the finger is seizing objects with linear edges. It should be noted that the shape adaptation capability must be kept to perform enveloping grasps if required (upper part of Fig. 7). The preshaping equation characteristic of a finger capable of pinch grasps is

$$\sum_{i=1}^{n} \theta_i = \frac{\pi}{2}. \tag{8}$$

In this case, this preshaping can be described by a single (and simple) equation. To achieve this feature, prototypes have been developped using various solutions such as a complex cam-linkage mechanism that can be disengaged (Bartholet, 1992), an additional linkage (Gosselin and Laliberté, 1996), or more recently, a combination of two interconnected

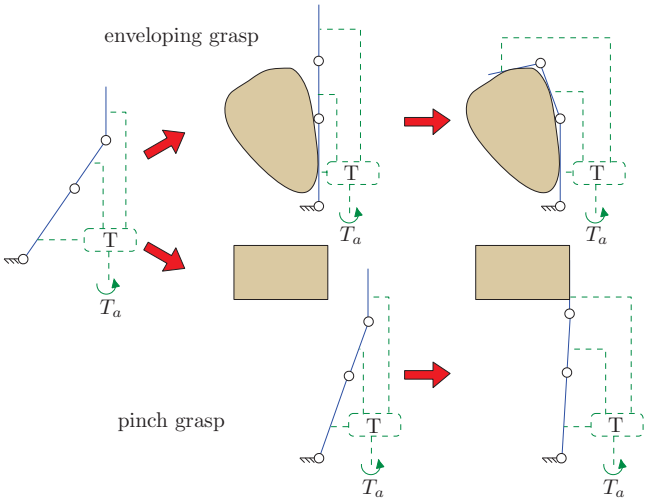

Figure 7. Two possible closing sequences of a three-phalanx finger designed to allow pinch grasps.

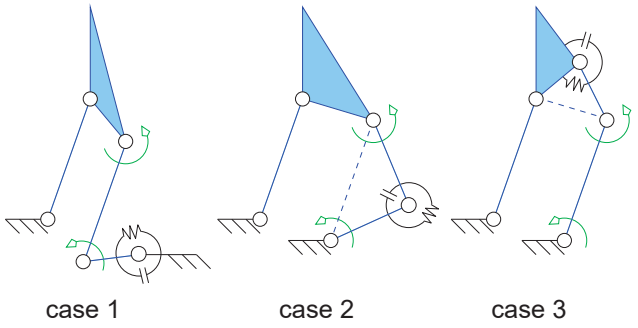

Figure 8. Designs of the two-phalanx class S architecture allowing pinch preshaping.

struts with non-reversible valves dubbed the *air parallelogram* (Bégoc et al., 2004). These solutions have been reported to work well but they all require an addition to the transmission linkage used for self-adaptation. However, if one carefully uses triggered elements in certain joint(s) of the mechanism, this behaviour can be closely approached without requiring any addition.

It is well known that a parallelogram linkage maintains its coupler link parallel to the ground. This property can be used in the design of self-adaptive robotic fingers with pinch preshaping. For instance, let us consider the mechanical architectures presented in Fig. 3. Non-trivial cases (1 – 3) can be very easily kinematically reduced to a parallelogram if simple geometric conditions on the lengths of the links are satisfied. Namely, in case 1 they are $b = l_1$ and $r = c$. In case 2, they become $c = d$ and $s = l_1$. Finally, in case 3 one has $a = l_1$ and $t = d$. If these conditions are satisfied, Eq. (2) becomes

$$\theta_1 + \theta_2 = \phi - \eta + \theta_2. \tag{9}$$

This equation is valid with any of the three cases considered and it is trivial to show that the right hand side of the previous equation is constant, i.e. θ_2 is canceled in all cases by η and only the design parameters are left. Therefore, it is possible to choose these parameters to exactly match Eq. (8). Hence, for the distal phalanx of a two-phalanx class S finger to maintain a constant orientation with respect to the ground, one simply has to place a triggered element in one joint of the transmission linkage, adjust the lengths of the latter in order for the resulting one-DOF mechanism to be a parallelogram and choose the remaining geometric parameters to ensure that Eq. (9) matches Eq. (8). The method is illustrated in Fig. 8, the green circular arrows indicate possible actuation location. With these designs, the distal phalanx will remain perpendicular to the palm until a contact occurs. When this contact is established, the actuation torque will overcome the preloading of the triggered element and initiate the closing of the other phalanx. Hence, pinch preshaping is achieved without any additional mechanisms.

Nevertheless, if the contact occurs with the distal phalanx during this pregrasping phase, the resulting grasp stability must be studied to determine if the linear contact can be maintained. Indeed, with a contact on only one phalanx, i.e. one constraint, a two-DOF finger without additional mechanisms is not necessarily in static equilibrium as discussed in Birglen and Gosselin (2004). If this is not the case, contact with the whole line will be lost and a sliding motion of the finger in contact with only one vertex of the object will occur. This contact situation can lead to either a stable grasp or ejection (Birglen and Gosselin, 2006b). It should be noted that the parallelogram linkages proposed in Fig. 8 are known to achieve very poorly with respect to grasp stability. However, this is not an issue here because the parallelogram shape is only maintained during the preshaping phase and pinch grasps. It is automatically disengaged when a contact does not occur with the distal phalanx.

Let us consider the case 2 of Fig. 8. The equilibrium equation is defined as a set of contact locations on the distal phalanx leading to a static equilibrium of the finger with no contact on the proximal phalanx, i.e. the set of k_2 such as $f_1 = 0$ (cf. Fig 5). Note that this situation corresponds to the desired pinch grasp. The equilibrium equation of the finger discussed here is

$$e(\theta_1, \theta_2) = k_2 = h_4 \cos \theta_2 \tag{10}$$

where h_4 is the signed distance between O_2 and the intersection of lines (O_1O_2) and (O_3O_4). The equilibrium equation value e is a particular location of the contact force on the distal phalanx (not the value of the force but its location) and a function of h_4 which is itself a complex function of θ_1 and θ_2. The equilibrium equation defines a set of contact locations (a surface) in the grasp-state space $(\theta_1, \theta_2, k_2)$. Note that its value can be smaller than zero or greater than l_2, i.e. outside the physical limits of the phalanx. The equilibrium equation

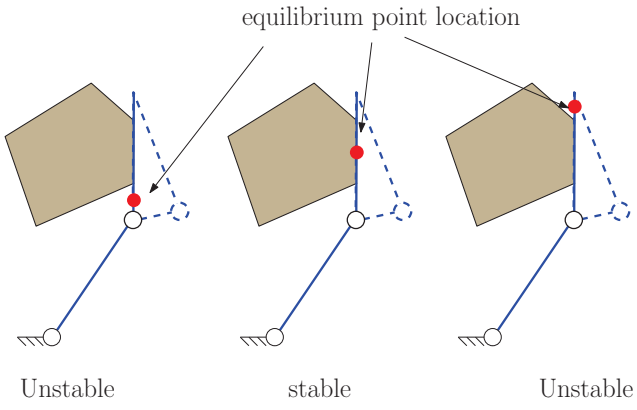

Figure 9. Stability of a planar pinch grasp depending on the equilibrium location.

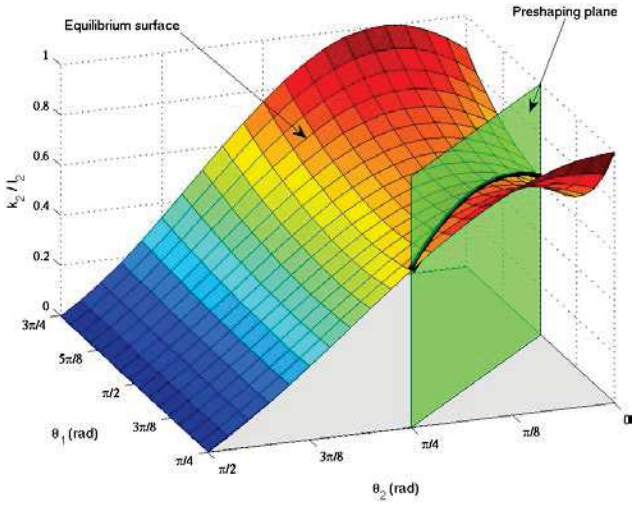

Figure 10. Equilibrium surface of the optimal design of two-phalanx finger with pinch preshaping.

is critical with respect to the grasp stability of a linear contact. It has also been demonstrated in Birglen and Gosselin (2006b) that a linear contact with the distal phalanx of a two-phalanx self-adaptive finger is stable if and only if the location of the equilibrium position is located between both vertices of the line (cf. Fig. 9). However, it should be noted that if this condition cannot be met, ejection will not necessarily occur. Indeed, the grasp can still be stable if $e(\theta_1,\theta_2) < l_2$ but with a contact maintained only with one of the edges of the object.

Therefore, the stability of a linear grasp cannot be guaranteed in all cases, since the object cannot be assumed to have a linear contact with the entire distal phalanx. However, in most common cases, the linear contact is long enough to exceed the physical limit of the distal phalanx, i.e. the rightmost case of Fig. 9 can be disregarded, and a compromise can be found. This compromise lies between the avoidance of ejection, favored by a small value of the equilibrium location, and the ability to perform pinch grasp, favored by a large value of the equilibrium location. This compromise can be part of the optimization procedure characterized by an index I_e^*:

$$I_e^* = \begin{cases} 0 & \text{if} \quad \max(e)_W > l_2 \\ \min(e/l_2)_{W^*} & \text{otherwise} \end{cases} \tag{11}$$

where W^* is the set of phalanx angles during the preshaping, i.e. the locus described by $\theta_1 + \theta_2 = \pi/2$. This performance index is to be maximized. It ensures that the equilibrium value e is the closest possible to l_2 over the workspace W^* (its minimal value is maximized) without being greater than l_2 (the score drops to zero).

If the lengths of the proximal and distal phalanges are respectively chosen as 1 and $l_1/\sqrt{2} = 0.707$. The first step of the optimization is to find out an initial estimate of the geometric parameters. This initial choice can be done very easily by choosing the parameters to form a parallelogram. Then a numerical optimization toolbox can be used to further refine the design. Taking into account the constraints mentioned above, one can reduce the original set of 8 geometric parameters to only four: α, a, b and c in case 2 (since $\psi = \pi/2 - \alpha$ and $d = c$) to speed up calculations. An example of the result of such an optimization procedure is presented in Table 2 corresponding to the equilibrium locus illustrated in Fig. 10. Note that the set of angles θ_1 and θ_2 during the preshaping phase, denoted W^*, corresponds to a plane in the grasp-state space and the associated values of the equilibrium locations – maximized through the index I_e^* – are outlined in black in Fig. 10. The maximal value of the equilibrium equation over the workspace W does not exceed 1. Hence, no ejection occurs and the finger is always stable. The minimal value of the equilibrium equation in the preshaping phase W^* is 62.1% of l_2. This means that any linear contact with one vertex below $0.621 l_2$ and the other beyond the limit the phalanx is stable. This behaviour has been verified with a virtual prototype using a dynamic simulation package.

Table 2. Two-phalanx finger optimal geometric parameters.

ψ	a	b	c	d	α
95°	0.84	1.32	0.39	0.39	−5°

The procedure leading to this two-phalanx design can be adapted to a finger with three phalanges by taking into account the grasp stability and the expressions of the contact forces of three-phalanx fingers (Birglen and Gosselin, 2006a). Furthermore, it should be emphasized that this method is actually not limited to one class of kinematic architectures (the class S in this example). In order to maintain the desired orientation of the distal phalanx, one can use cascaded parallelograms as illustrated in Fig. 11. In this figure, three architectures from Birglen (2009) are illustrated

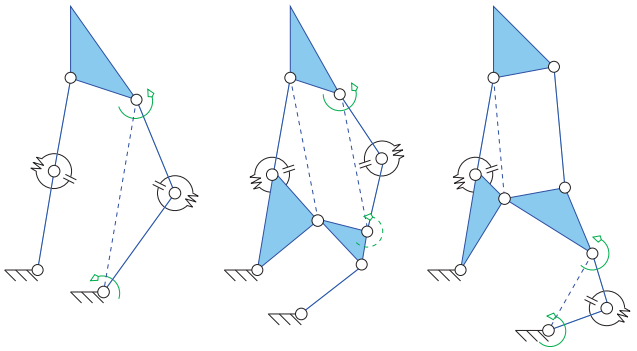

Figure 11. Three-phalanx self-adaptive fingers with pinch preshaping.

where two triggered elements are used to maintain the orientation of the distal phalanx during the closing preshaping. The green circular arrows indicate possible actuation location, but it should be noted that only one location has to be chosen, i.e. all three fingers have three DOF but can be driven by a single actuator.

3.3 Anthropomorphic preshaping

When designing prosthetic fingers, two approaches are possible. Either attention is paid to the closing motion of the prosthesis to mimic a human finger, i.e. an *anthropomorphic preshaping* (Figliolini and Ceccarelli, 2002; Ceccarelli et al., 2006b,a), or to the forces generated by the phalanges (de Visser and Herder, 2000). Since the latter approach does not require a particular closing motion, it has lead to the introduction of self-adaptive fingers in prosthetics (de Visser and Herder, 2000; Lotti and Vassura, 2002; Carrozza et al., 2004). However, it is possible to design an artificial finger that has an anthropomorphic closing motion while keeping the self-adaptation property as also very recently proposed in Wu et al. (2009). In Figliolini and Ceccarelli (2002), it is illustrated that in the absence of obstacles, the closing motion of a human finger exhibits approximately linear relationships between the rotations of the individual phalanges. Namely, one has

$$\theta_i = m_1(\theta_p - \pi/2) \quad \text{and} \quad \theta_d = m_2(\theta_p - \pi/2), \tag{12}$$

where $(\theta_p,\theta_i,\theta_d)$ are respectively the proximal, intermediate and distal relative angles between the phalanges. Numerical values reported in Figliolini and Ceccarelli (2002) are used in this paper, i.e. $(m_1,m_2) = (3.96,2.37)$ with $90° \le \theta_p \le 197°$. Using again the two-phalanx finger illustrated in Fig. 5, the mechanism is reduced to a four-bar linkage by locking one joint to approximate the motion described by Eq. (12). If the resulting four-bar linkage is used to drive the last two phalanges of a prosthetic finger, i.e. $\theta_1 = \theta_i$ and $\theta_2 = \theta_d$, the preshaping equation is

$$\theta_2 = m\theta_1 \quad \text{with} \quad m = m_2/m_1. \tag{13}$$

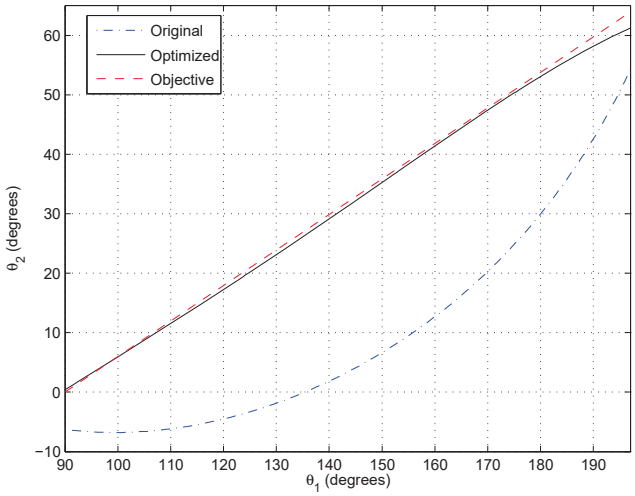

Figure 12. Comparison of preshaping motions.

Table 3. Two-phalanx finger second optimal geometric parameters.

ψ	a	b	c	d	α
119°	0.94	0.81	0.29	0.20	−149°

It is obvious that Eq. (2) is highly nonlinear and cannot usually be reduced into Eq. (13). However, a performance index measuring the closeness of the desired preshaping to the actual motion can be used, e.g.

$$I_a = \frac{1}{W^*}\int_{W^*} \frac{1}{1+\left(\dfrac{f^*(\theta_1)}{m\theta_1}-1\right)^2} d\theta_1 \tag{14}$$

where $f^*(\theta_1)$ is the solution of Eq. (2) for θ_2. Again, in the case of a four-bar linkage it is interesting to note that a closed-form expression of $f^*(\theta_1)$ exists (McCarthy, 2000) although its expression is impractical. The workspace of the finger is defined here as $W = \{90 < \theta_1 < 197°, 0 < \theta_2 < 64°\}$ to match the workspace proposed in Figliolini and Ceccarelli (2002) and I_a is therefore evaluated for $W^* \equiv 90 < \theta_1 < 197°$. If the joint locked during the preshaping is O_4 (case 2 in Fig. 8) the same optimization procedure discussed in the previous section yields the results presented in Table 3. Again, these parameters have been obtained with $l_1 = 1$ and $l_2 = l_1/\sqrt{2} = 0.707$. This time, the initial estimate has been chosen geometrically to have approximately the desired initial and final position, disregarding intermediate behaviour. A comparison of the initial, optimal and desired preshaping motions is illustrated in Fig. 12.

The equilibrium surface associated with this optimal set of geometric parameters is illustrated in Fig. 13. Equation (2) for any value of k_2 defines in this grasp-state space a preshaping surface illustrated in Fig. 13. Note that ideally, this surface should be a plane as the objective of the optimization

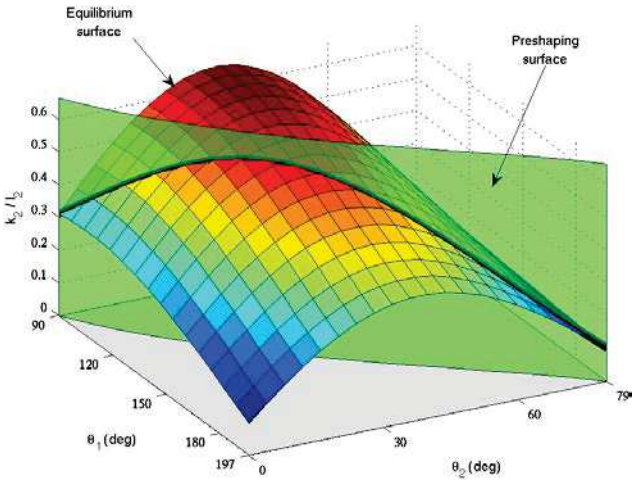

Figure 13. Equilibrium surface of the optimal design of two-phalanx finger with anthropomorphic preshaping.

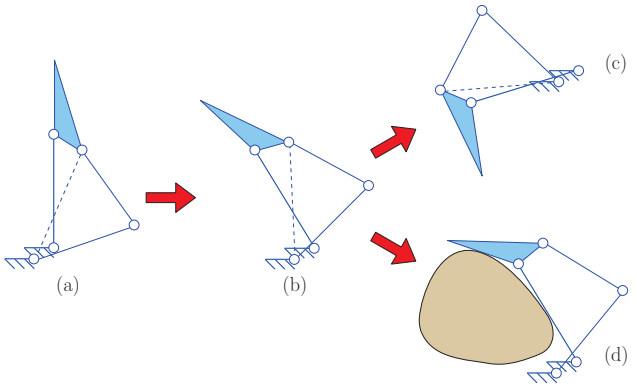

Figure 14. Possible closing motions of the optimized finger.

procedure was to approach Eq. (13). The finger built with these parameters and with a triggered passive element in O_4 will have a preshaping close to a human finger while keeping the self-adaptation property as illustrated in Fig. 14.

4 Conclusions

The issue of the kinematic preshaping of linkage-driven self-adaptive finger was discussed in this paper. A general method was proposed to achieve various preshapings based on using triggered passive elements. These elements reduce the number of DOF of self-adaptive fingers to one and allow to study the motion undergone by these fingers when no contact has occurred. Based on basic kinematic properties of four-bar linkages, designs of self-adaptive fingers were proposed that allow pinch grasps without requiring any additional mechanisms. The method was subsequently used in another example aiming at mimicking the closing motion of a human finger. These two examples of preshapings were demonstrated

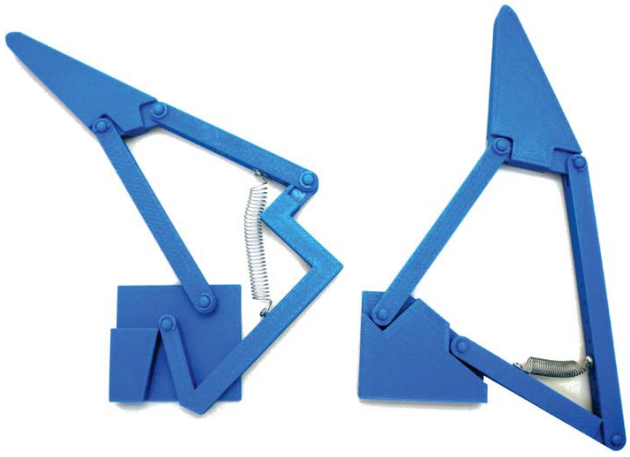

Figure 15. Prototypes of self-adaptive fingers with the discussed preshapings.

experimentally during the 2010 IFToMM/ASME International Workshop on Underactuated Grasping using fused deposition models illustrated in Fig. 15. Finally, only two different types of preshaping were discussed in this paper and with only one simple class of self-adaptive fingers. However, it is probable that any kind of motion is achievable using other architectures of self-adaptive fingers and that the presented preshapings can also be achieved by most of these other architectures.

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